
Coupling of Microscopy and Thermomechanical Models to Explain the Extent and Location of TRIP Product in Simulated PBF-LB of Ti-1023

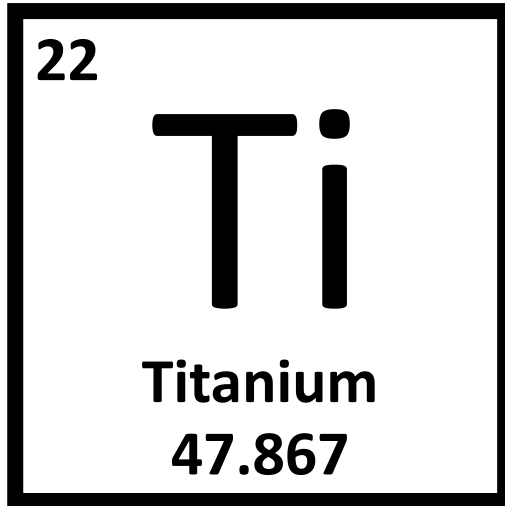
**Chris Jasien^a Alec Saville^a Kamel Fezzaa^b Tao Sun^b John Foltz^c
Kester Clarke^{a,d} Amy Clarke^{a,d}**

^a George S. Ansell Department of Metallurgical and Materials Engineering, Colorado School of Mines; Golden, CO, USA

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^c Allegany Technologies Incorporated Specialty Materials; Monroe, NC, USA

^d Sigma Manufacturing Sciences Division, Los Alamos National Laboratory; Los Alamos, NM, USA



High specific strength
Elevated temperatures
Difficult to machine
\$\$\$

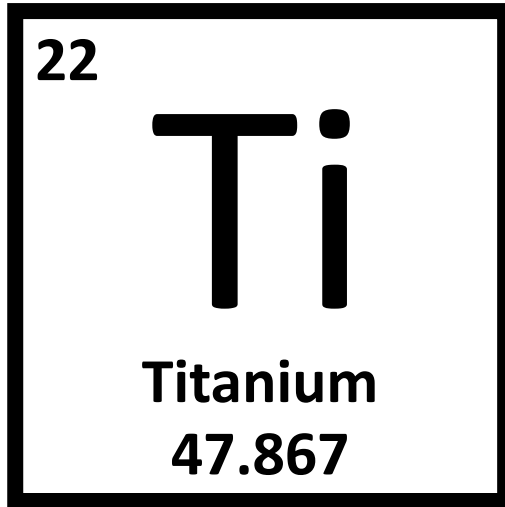
**Additive manufacturing of
aerospace/defense parts**

Ti-6Al-4V ($\alpha+\beta$ alloy) dominates AM

Extensively researched with robust microstructure-
processing relationships and legacy data

Thermal cycling presents some processing difficulties
(ie. residual stress cracking)





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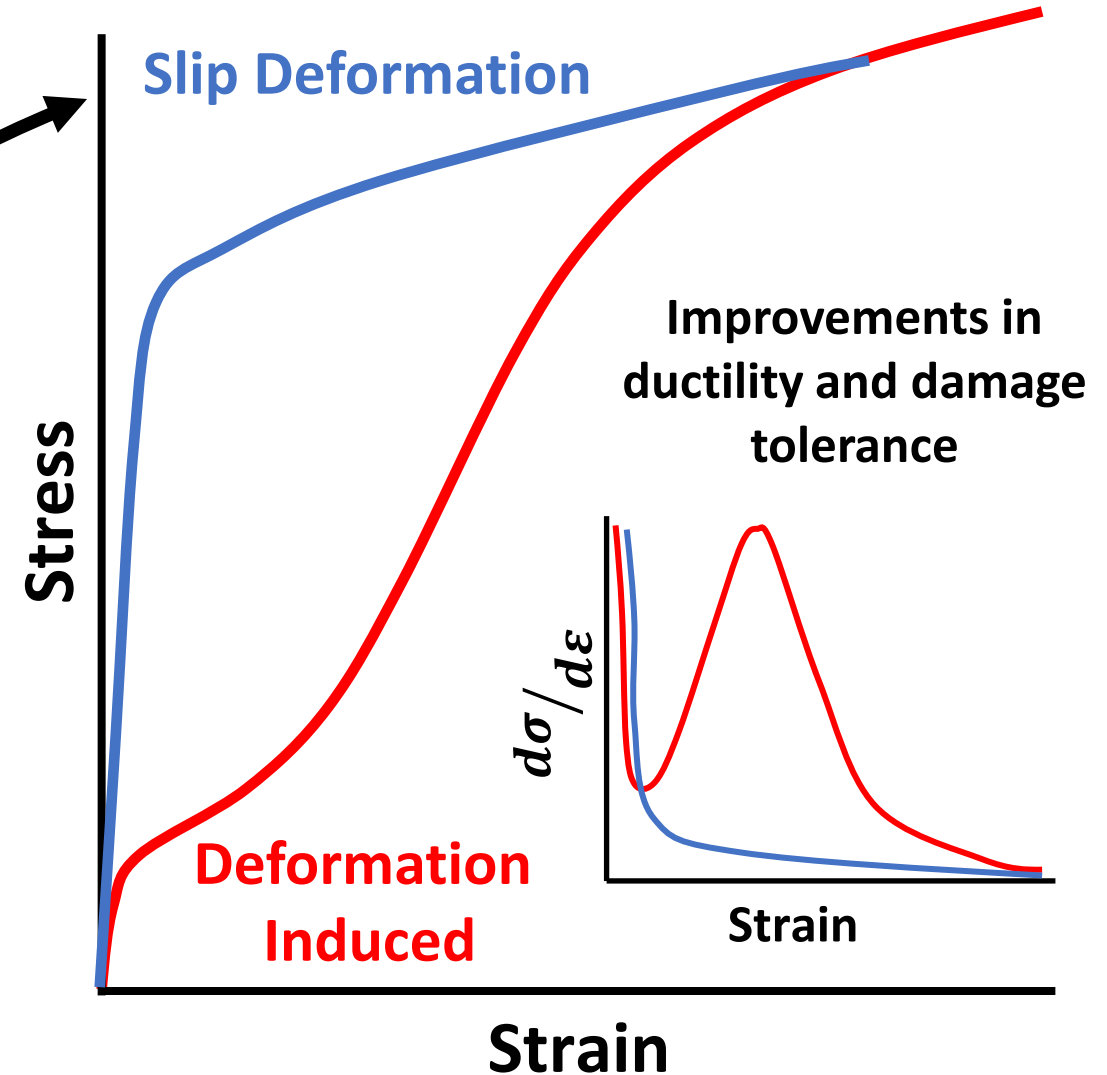
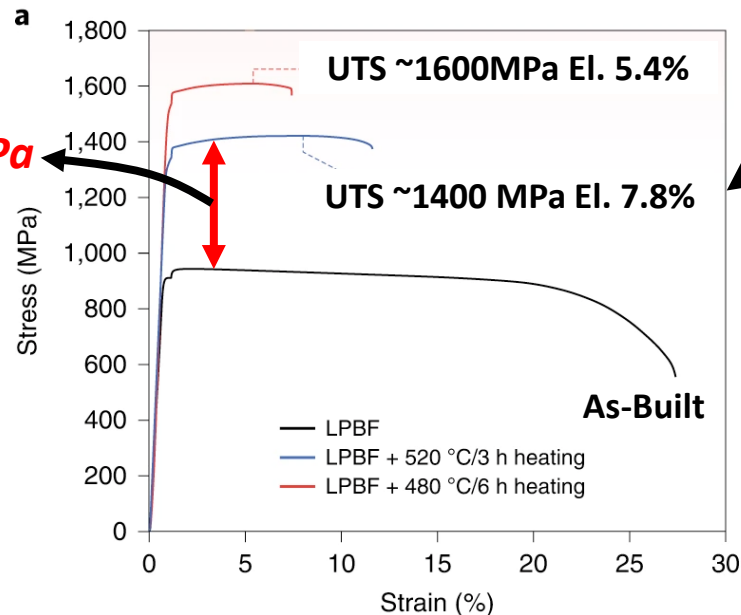


**Desire to utilize other
Ti alloys**

Metastable β -Ti

Class of titanium which retains high temperature β -phase after rapid cooling

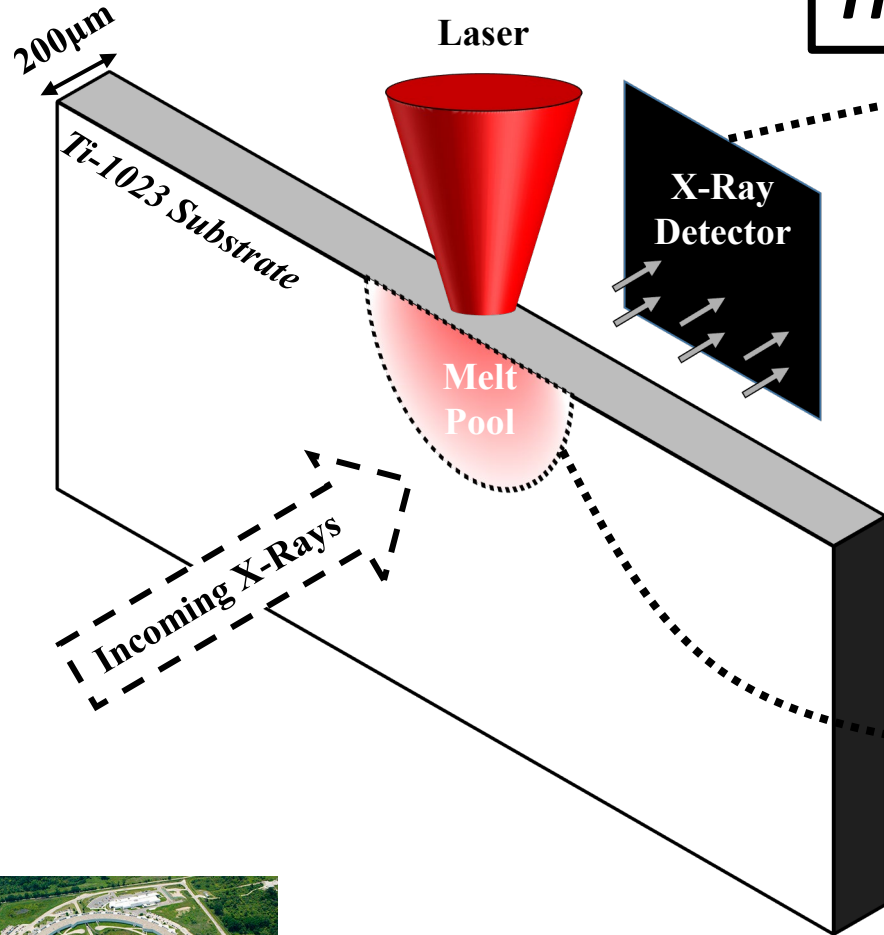
- Starting 'metastable' β microstructure facilitates enhanced properties
 - *Deformation induced transformations*
 - *High volume of precipitates*



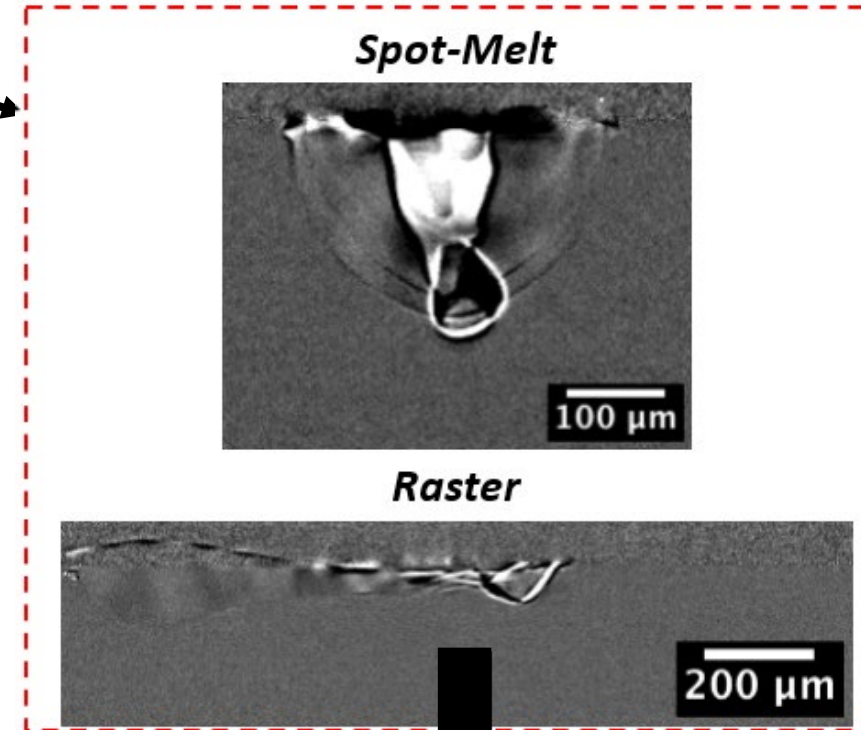
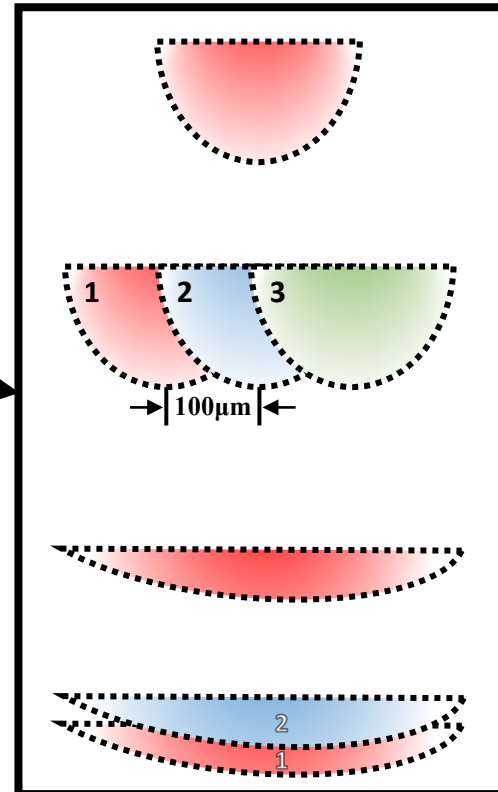
Experiments and Sample Fabrication

Investigated Alloy
Ti-10V-2Fe-3Al (wt.%)

Used to calibrate models



Scanning Strategies



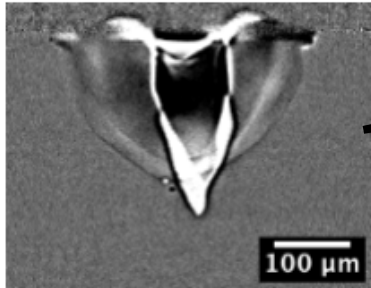
*Able to understand alloy
response at melt-pool scale*

**Advanced Photon Source
Argonne National Lab**

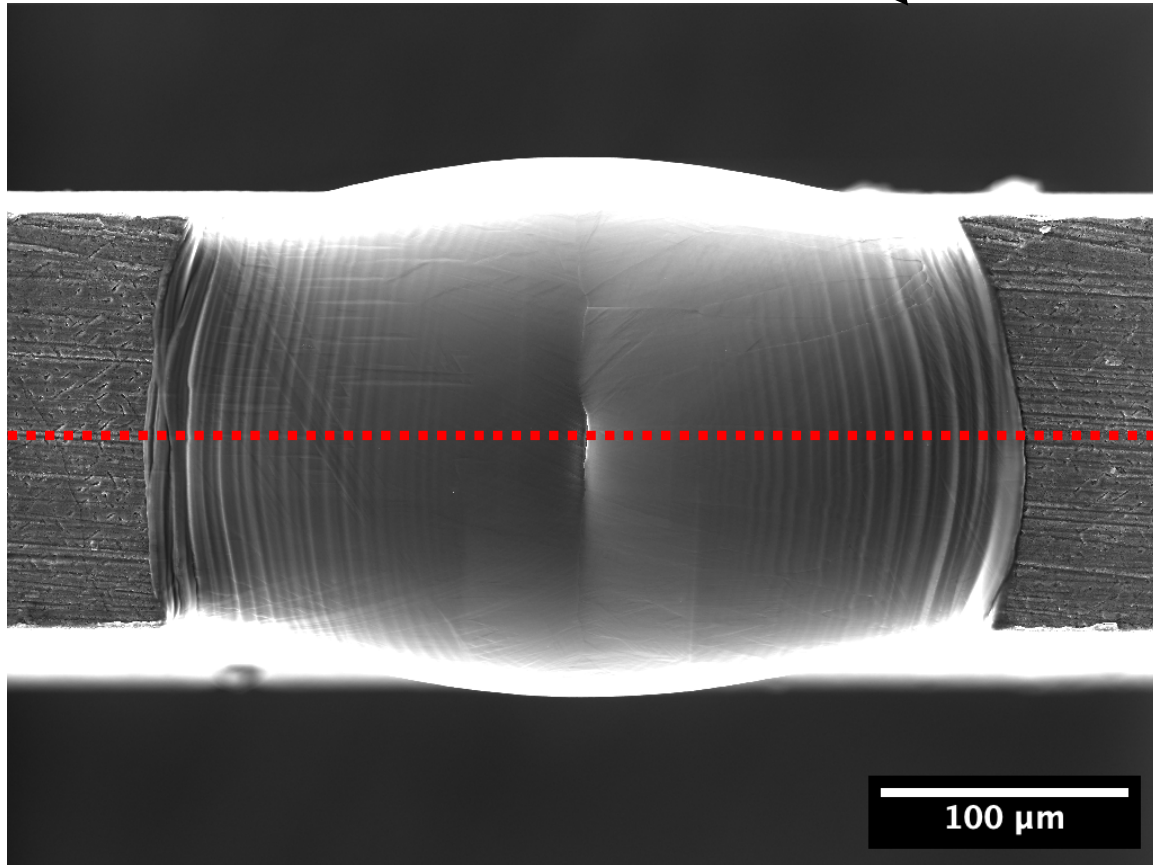


Single Spot-Melts

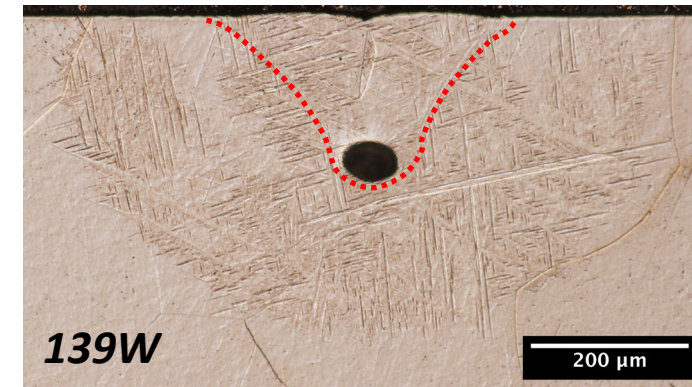
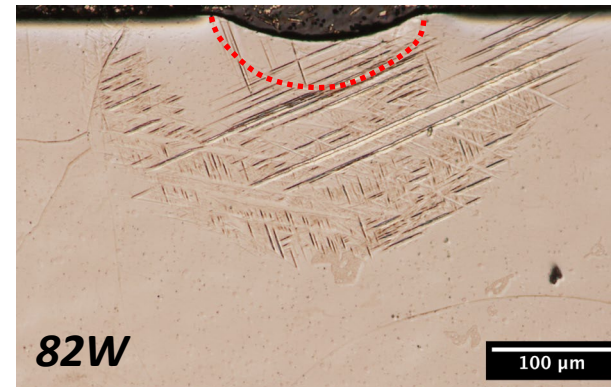
T.W. Duerig, et al., Formation and reversion of stress induced martensite in Ti-10V-2Fe-3Al, Acta Metallurgica 30 (1982) 2161–2172. [https://doi.org/10.1016/0001-6160\(82\)90137-7](https://doi.org/10.1016/0001-6160(82)90137-7).



Top-Down



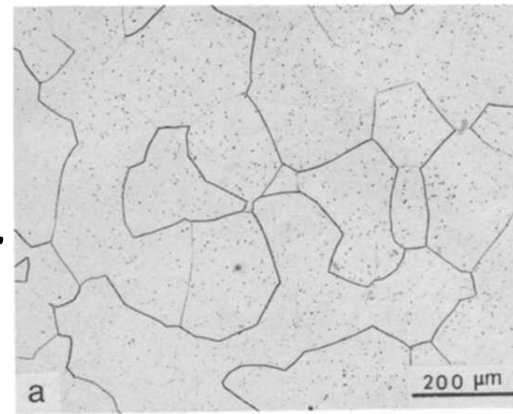
Cross-Section



Single Spot-Melts

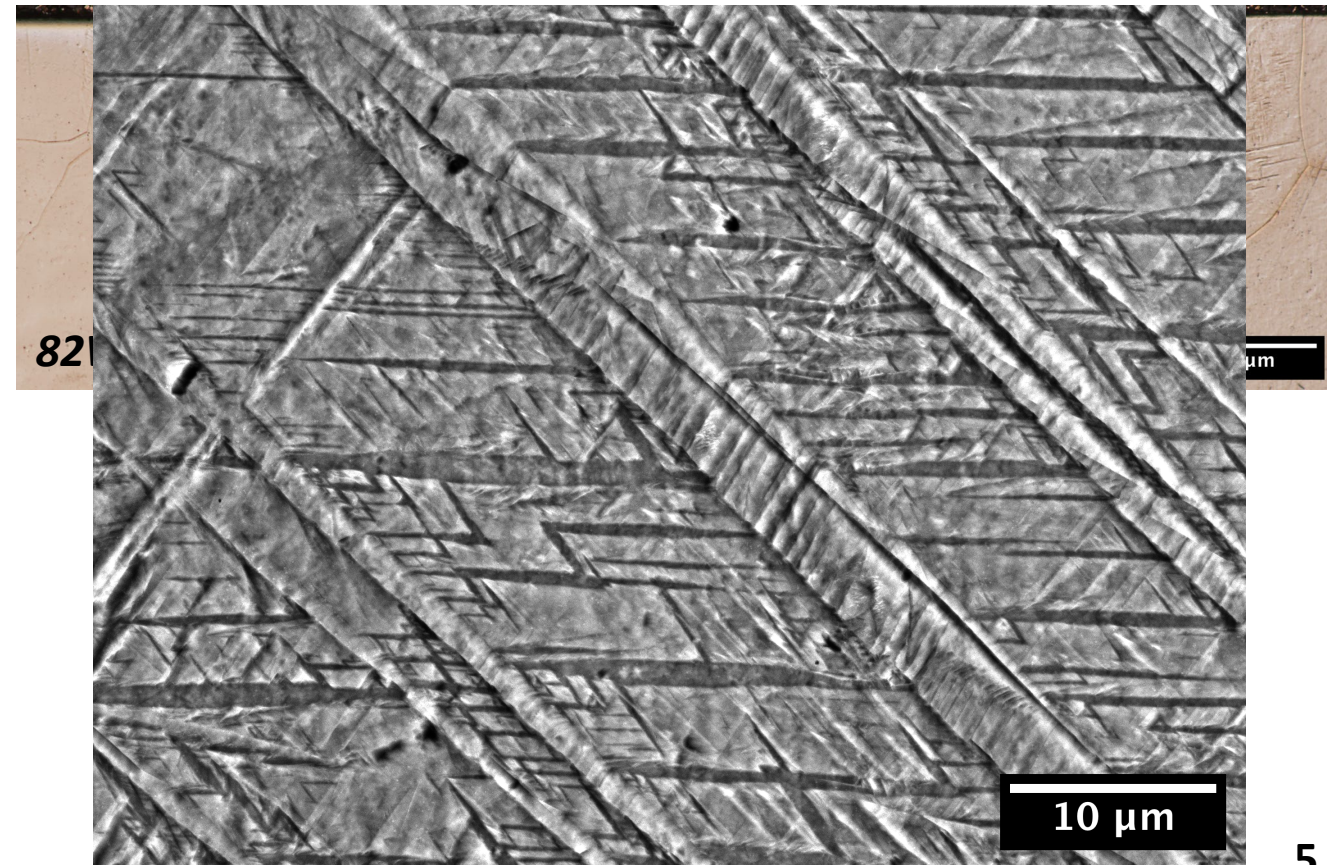
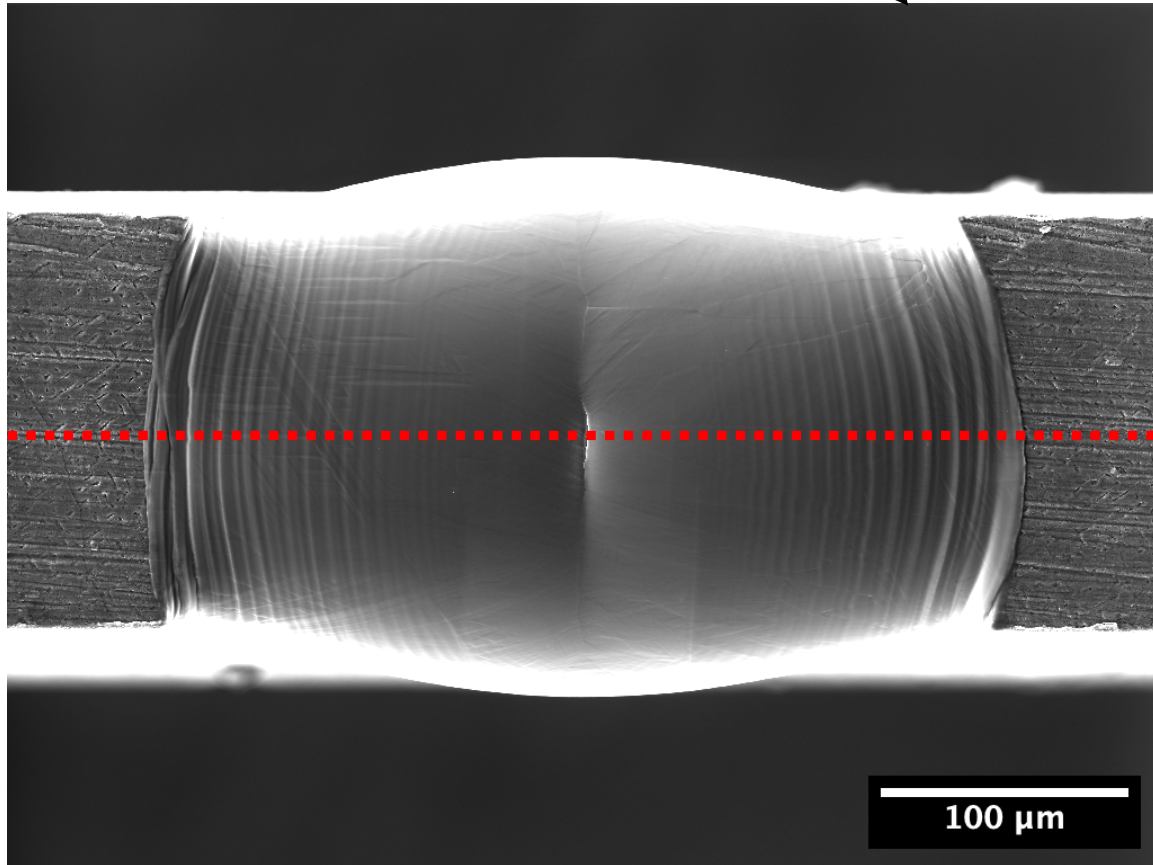
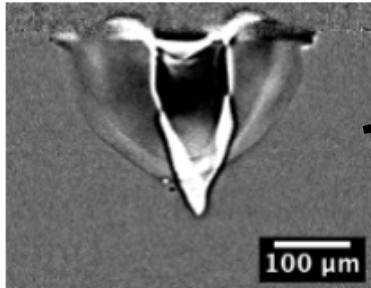
*We know quenched
Ti-1023 is single-phase...*

T.W. Duerig, et al., Formation and reversion of stress induced martensite in Ti-10V-2Fe-3Al, Acta Metallurgica 30 (1982) 2161–2172. [https://doi.org/10.1016/0001-6160\(82\)90137-7](https://doi.org/10.1016/0001-6160(82)90137-7).

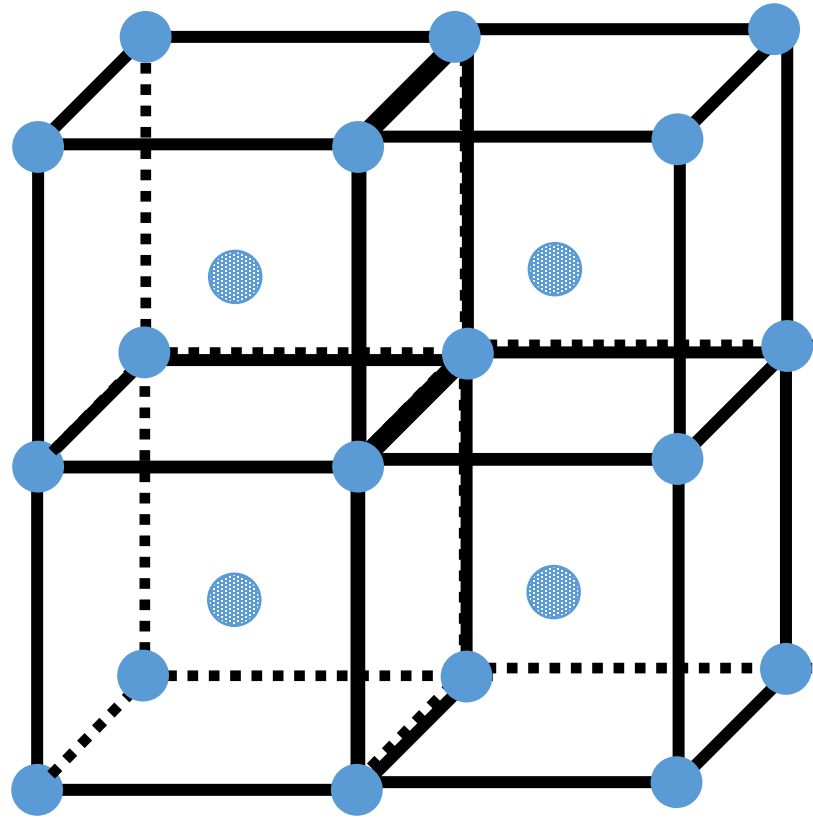


Cross-Section

Top-Down

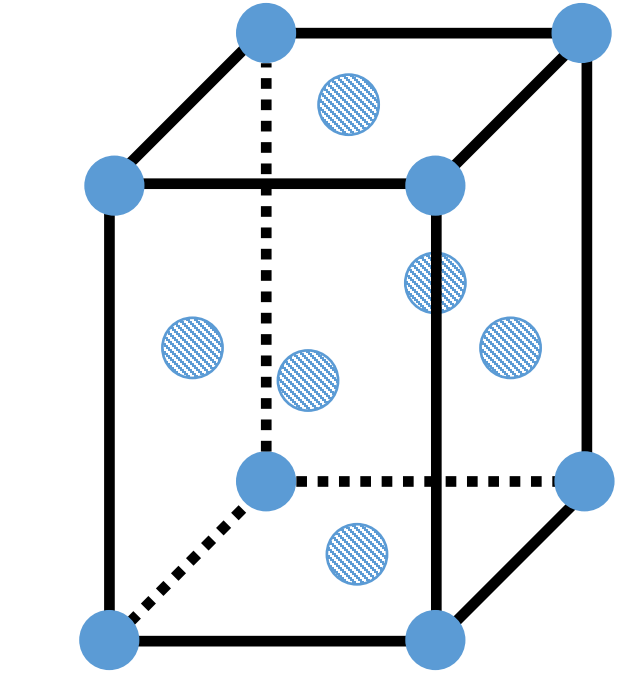
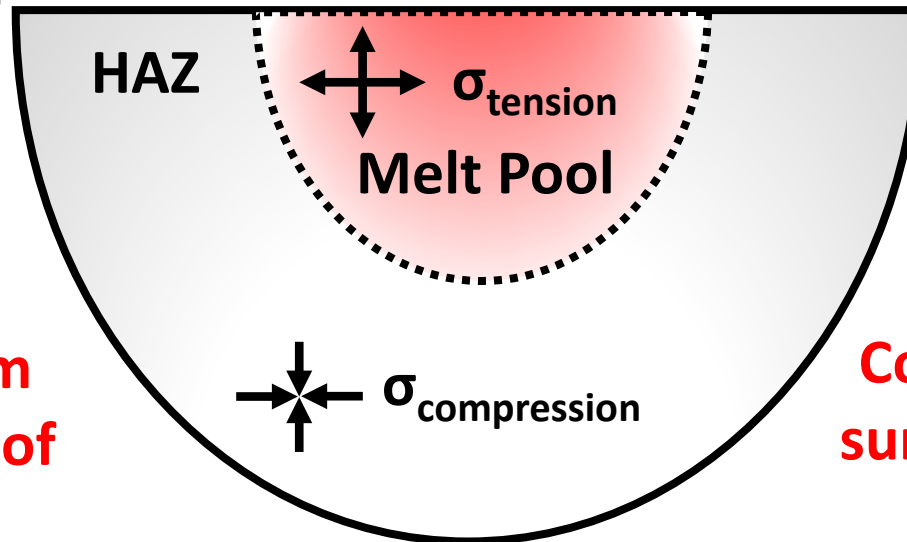
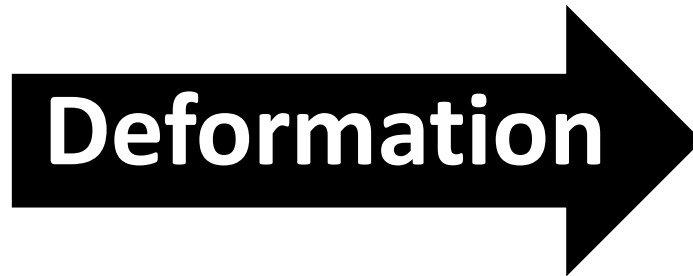


Transformation Induced Plasticity



BCC β -phase

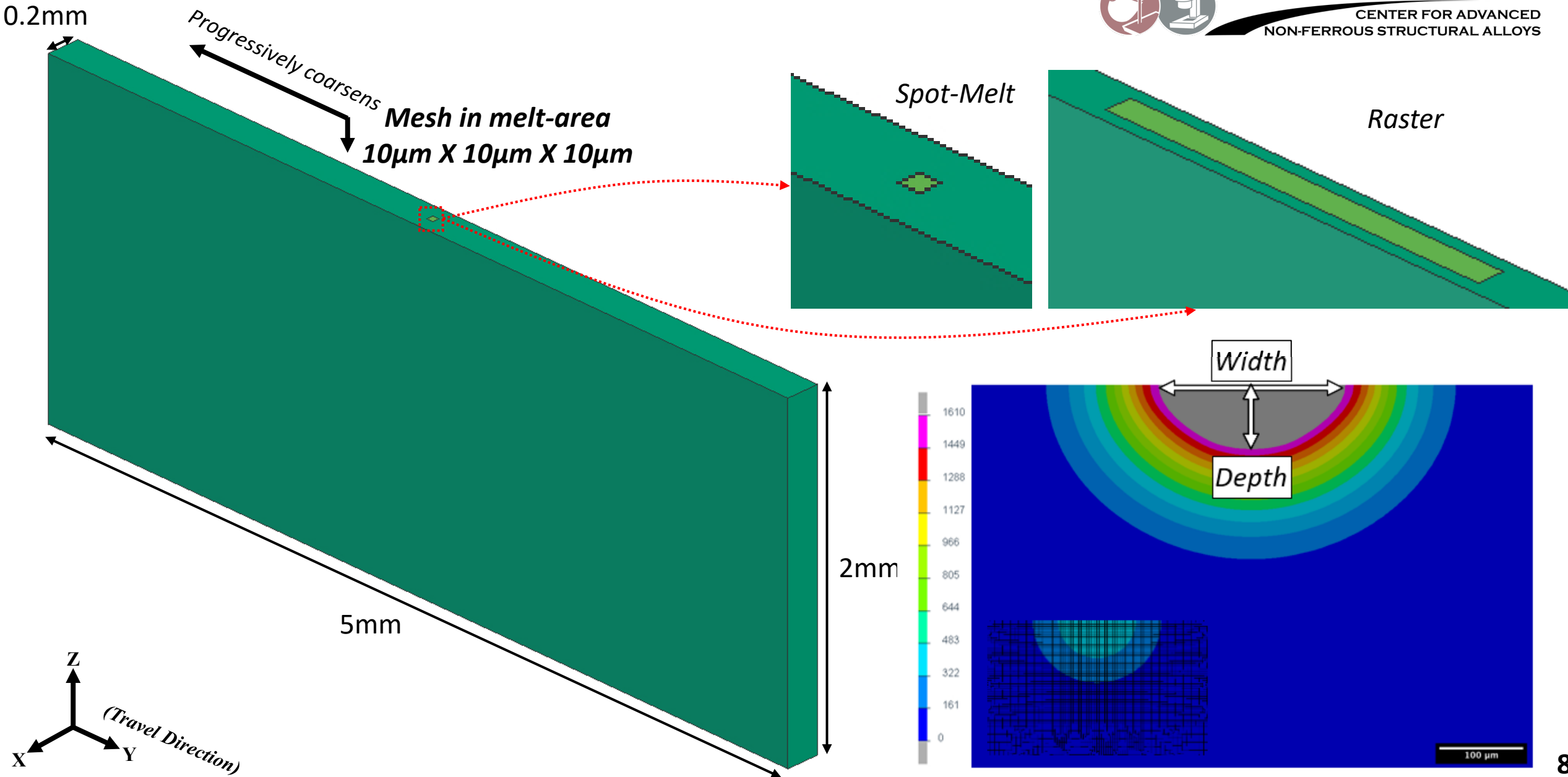
Tensile stresses from thermal contraction of melt-pool



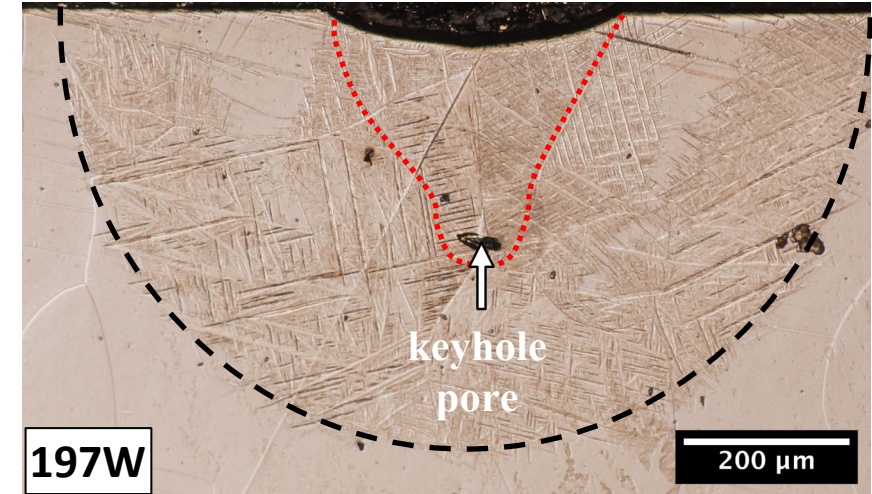
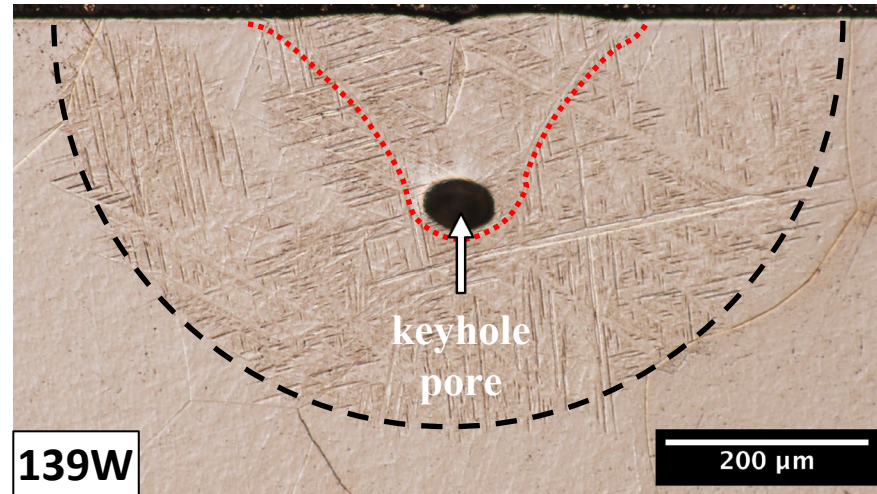
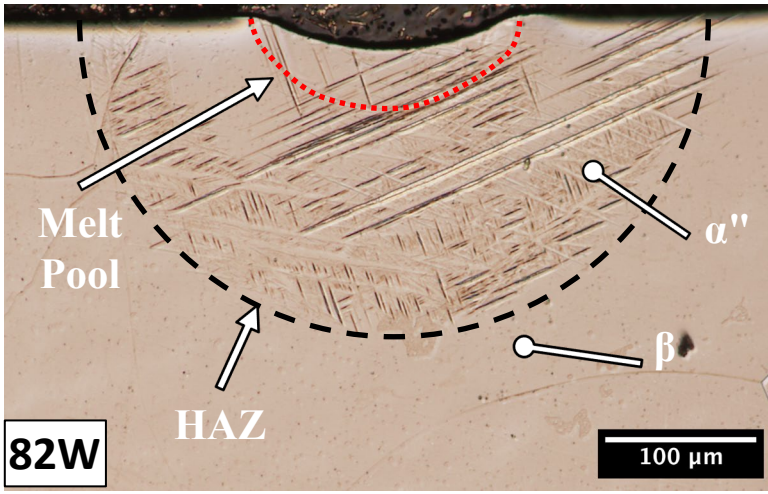
Orthorhombic α'' -phase

Compressive stresses from surrounding material inhibit this contraction

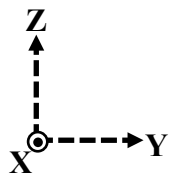
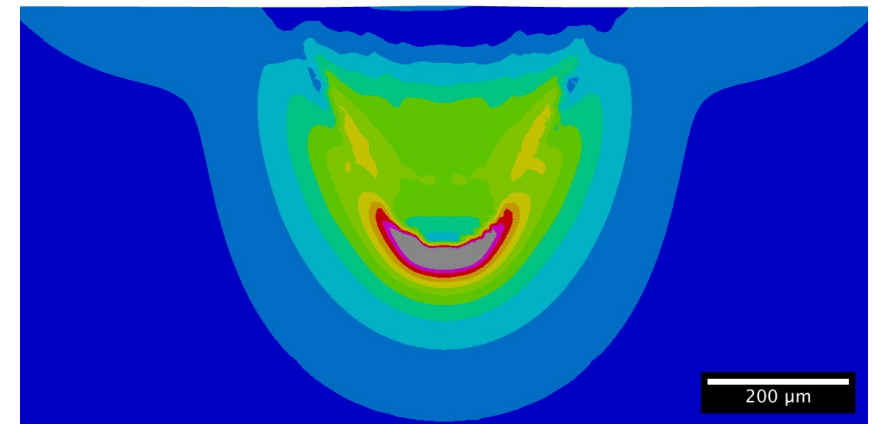
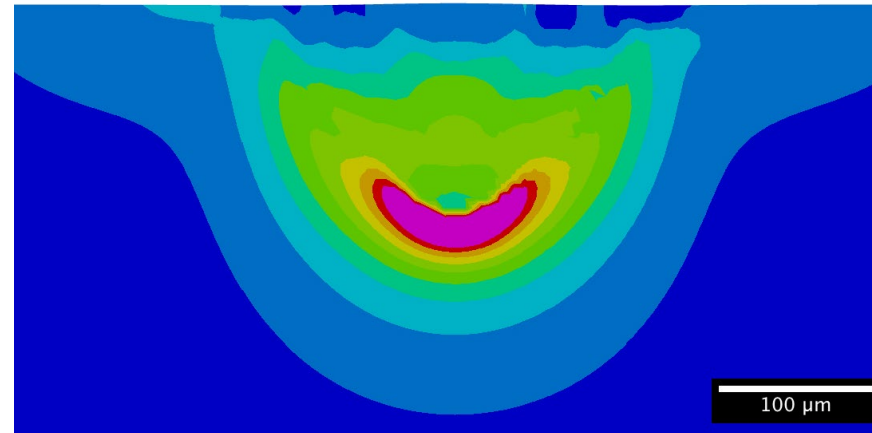
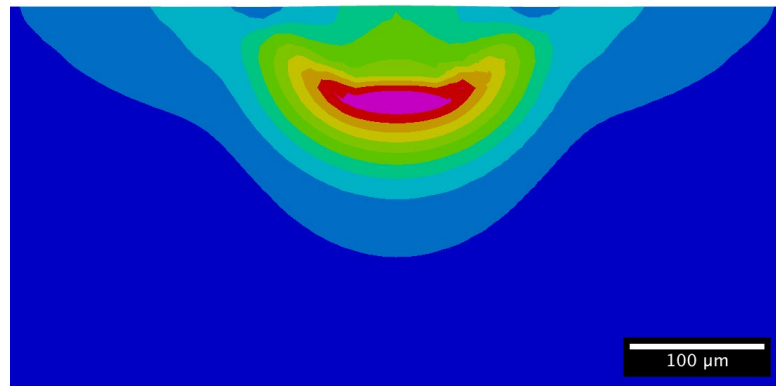
Thermomechanical Model - SYSWELD



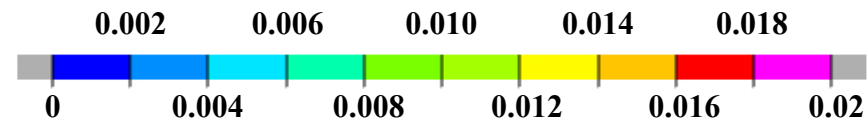
Single Spot-Melts



Thermomechanical Simulations (SYSWELD)

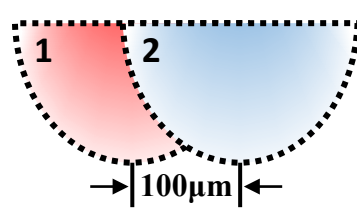


Von Mises Strain

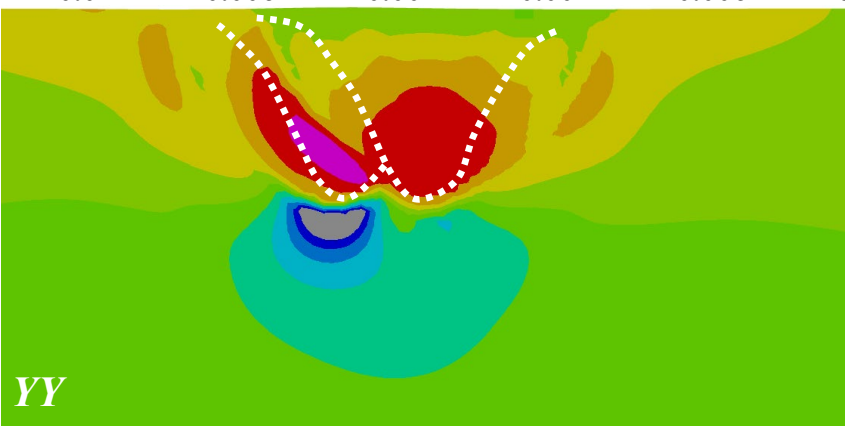
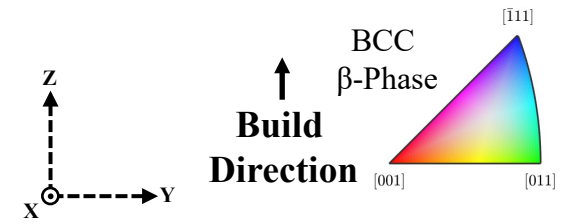
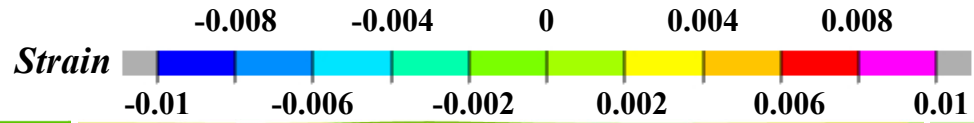
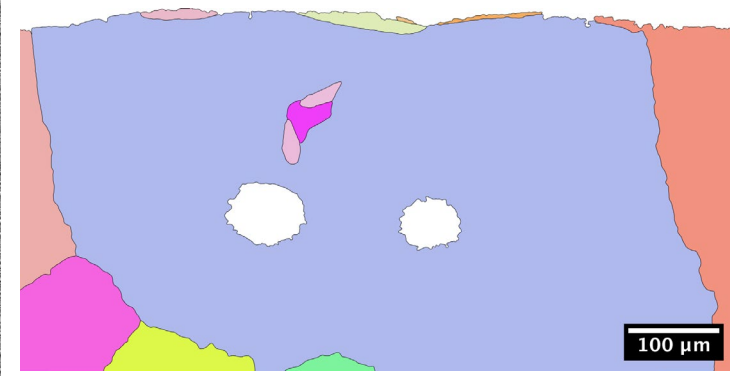
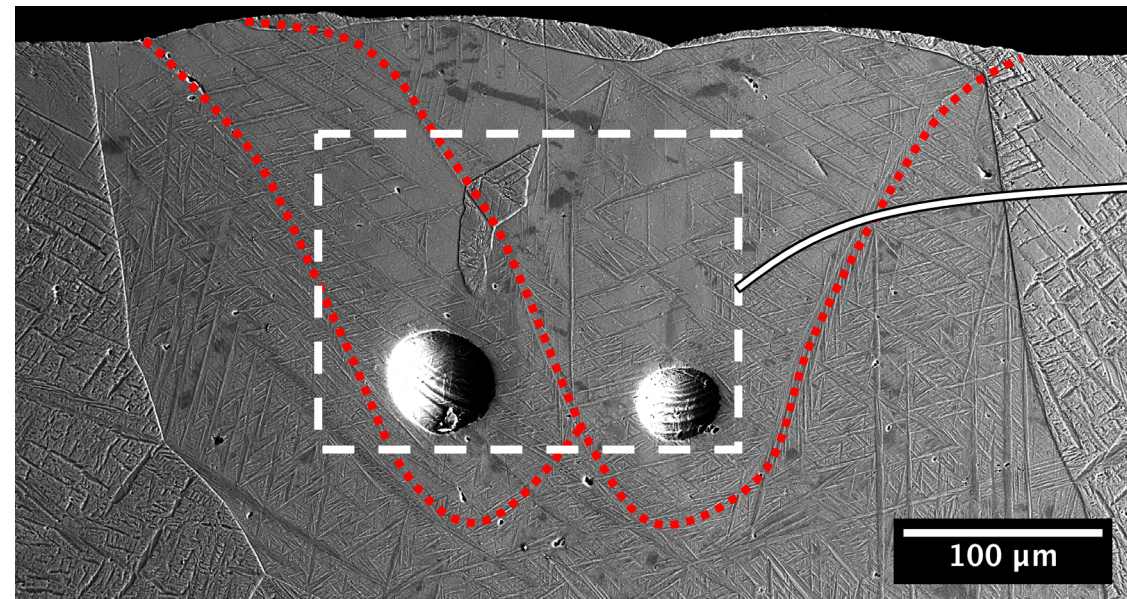


Overlapping Spot-Melts

139W Double Hit

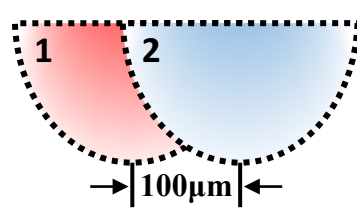


Cooled to RT before next spot-melt

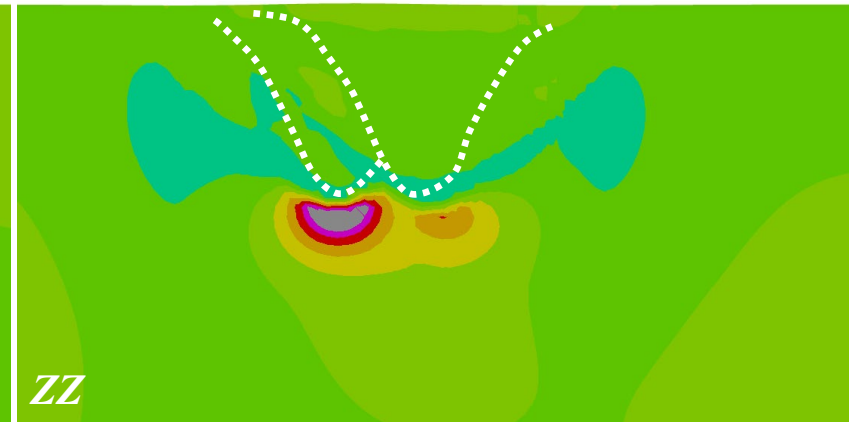
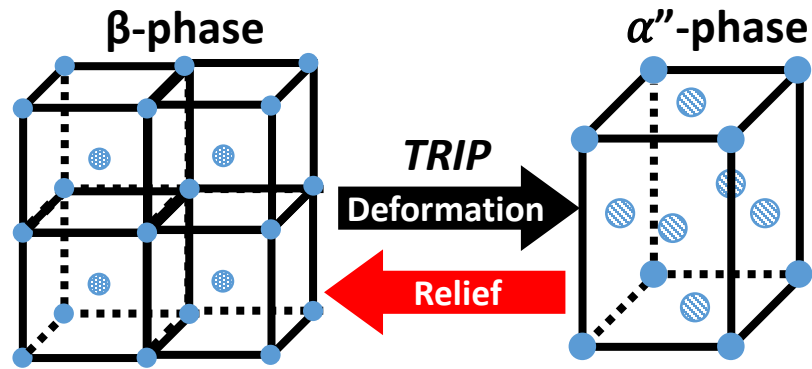
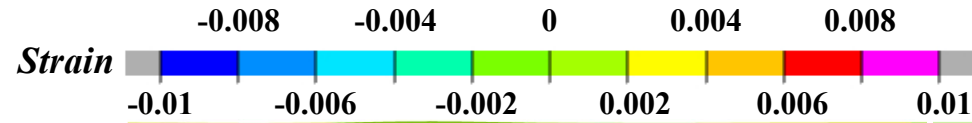
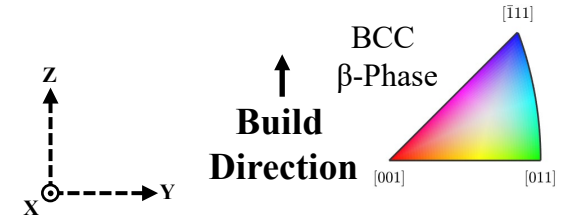
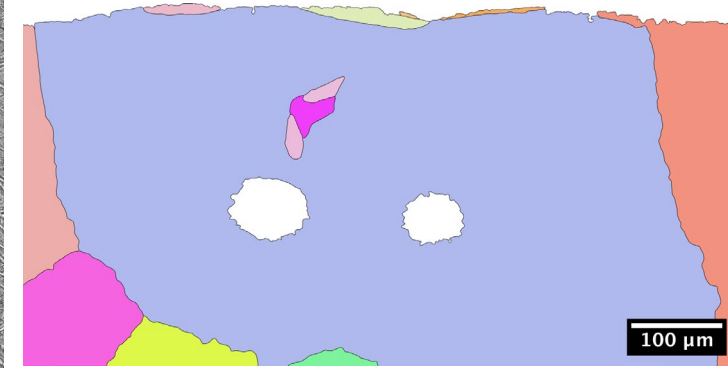
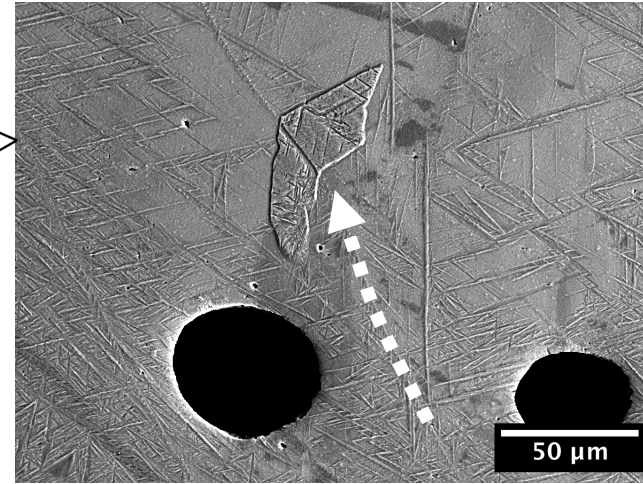
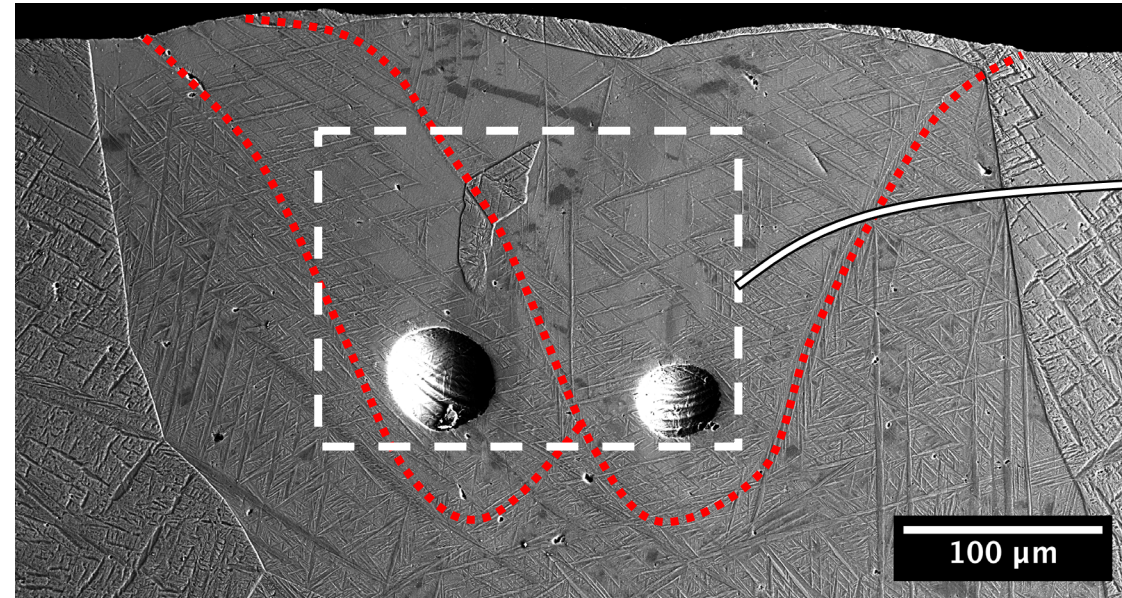


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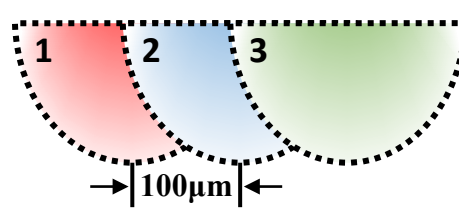


Cooled to RT before next spot-melt



Overlapping Spot-Melts

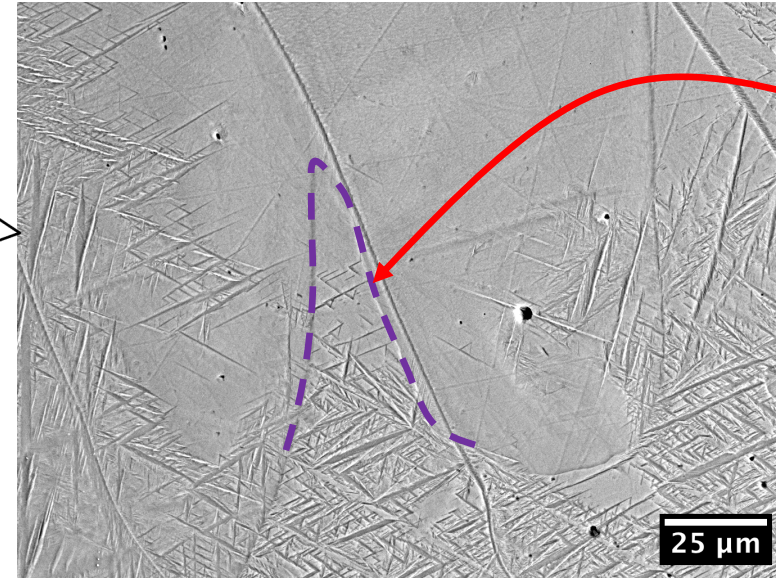
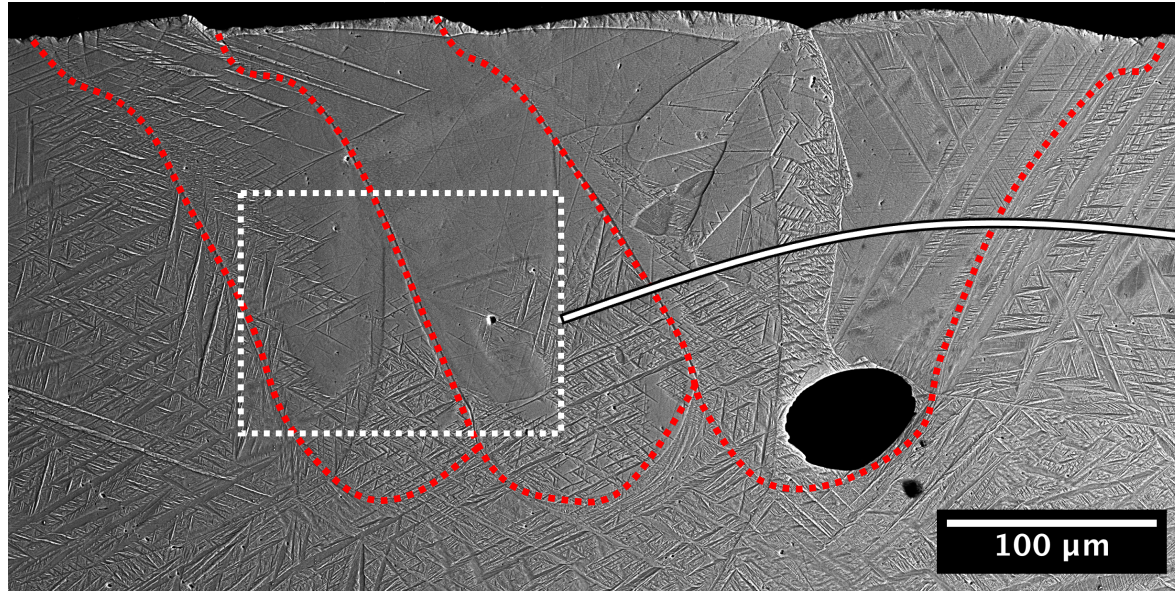
139W Triple Hit



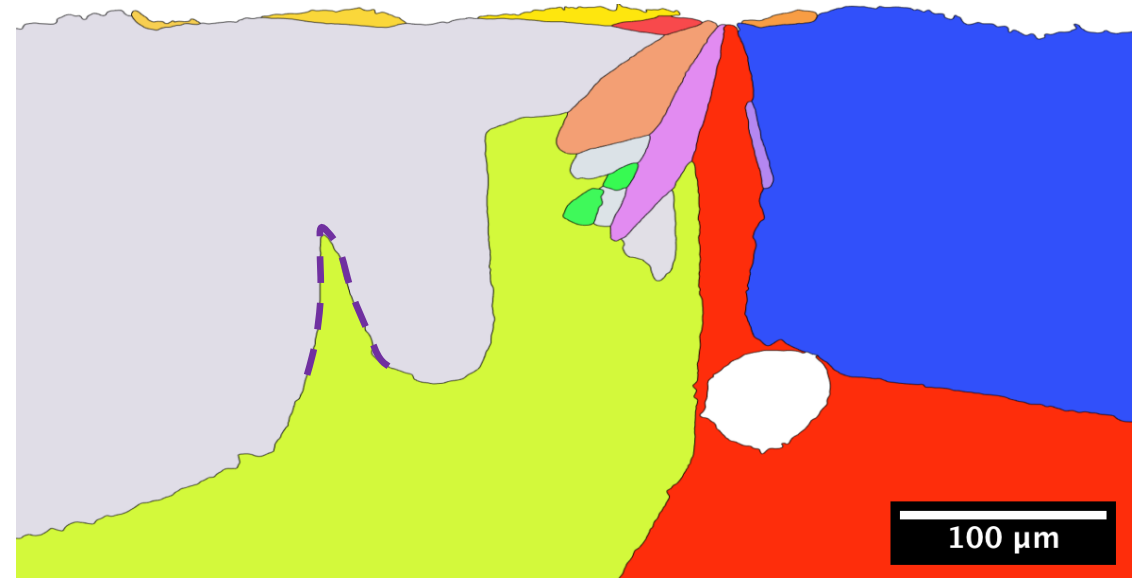
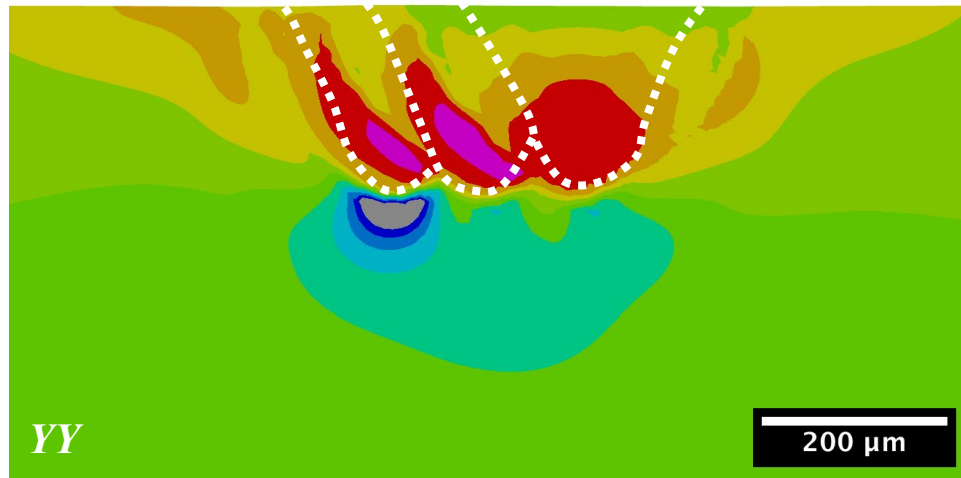
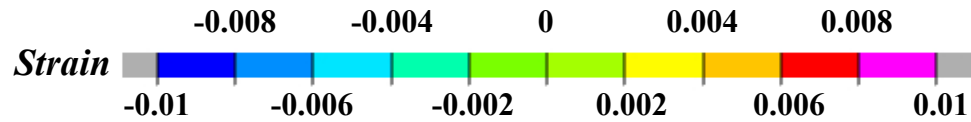
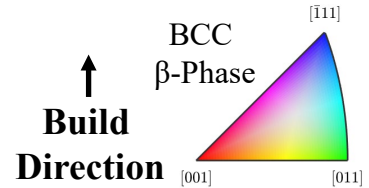
Cooled to RT before next spot-melt



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Abrupt α'' suppression



An Aside– Schmid Factor

*geometric factor controlling shear stress
on a specific slip system due to loading*

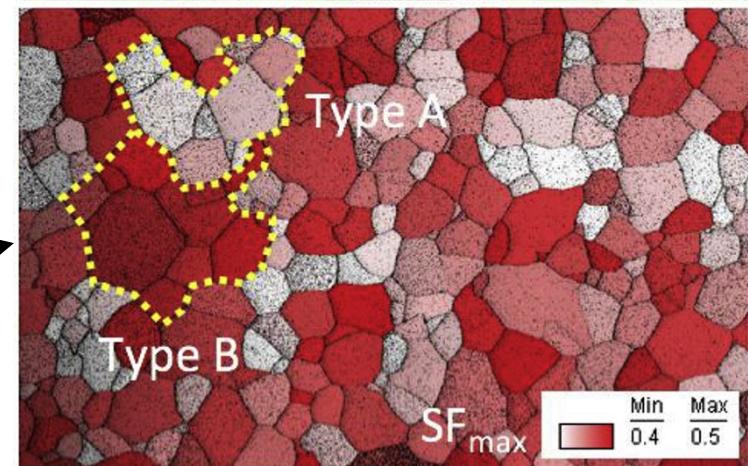
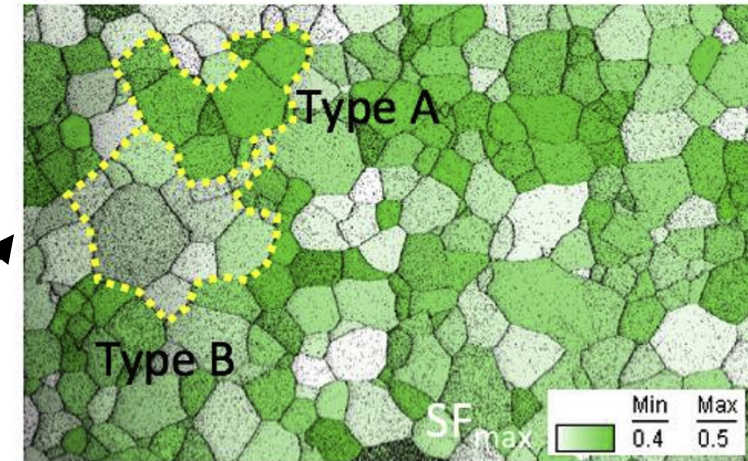
Schmid Factor used to predict deformation mechanism of each grain

BCC β -phase

$\{110\} \langle 1\bar{1}1 \rangle$ **Dislocation slip**

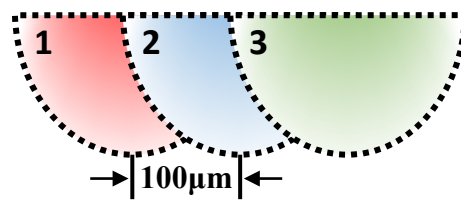
$\{112\} \langle 11\bar{1} \rangle$ **Martensite shear**

$\{332\} \langle 11\bar{3} \rangle$ **Twinning**



Overlapping Spot-Melts

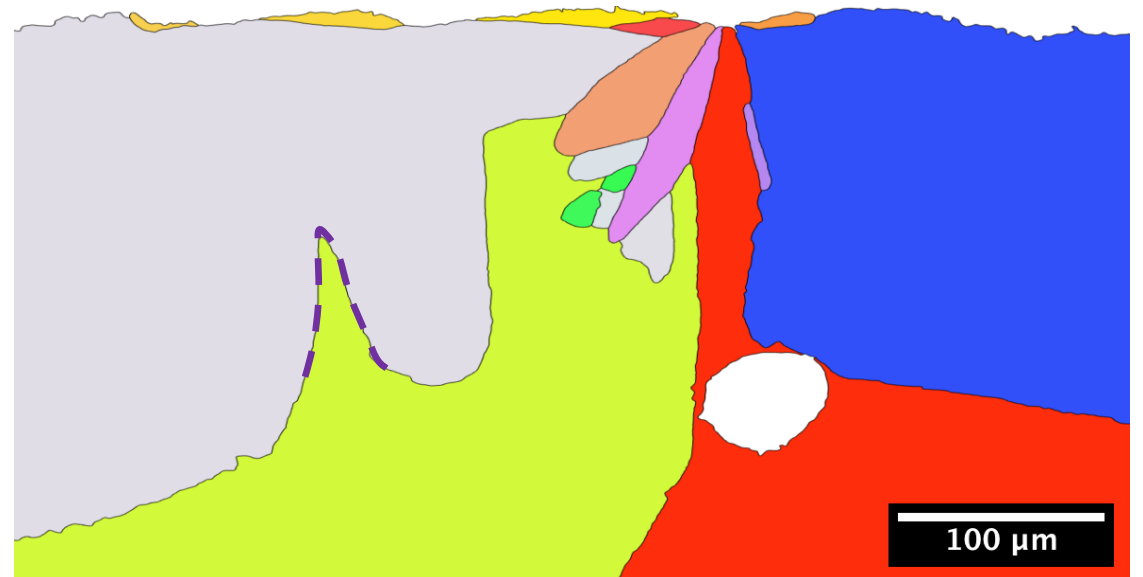
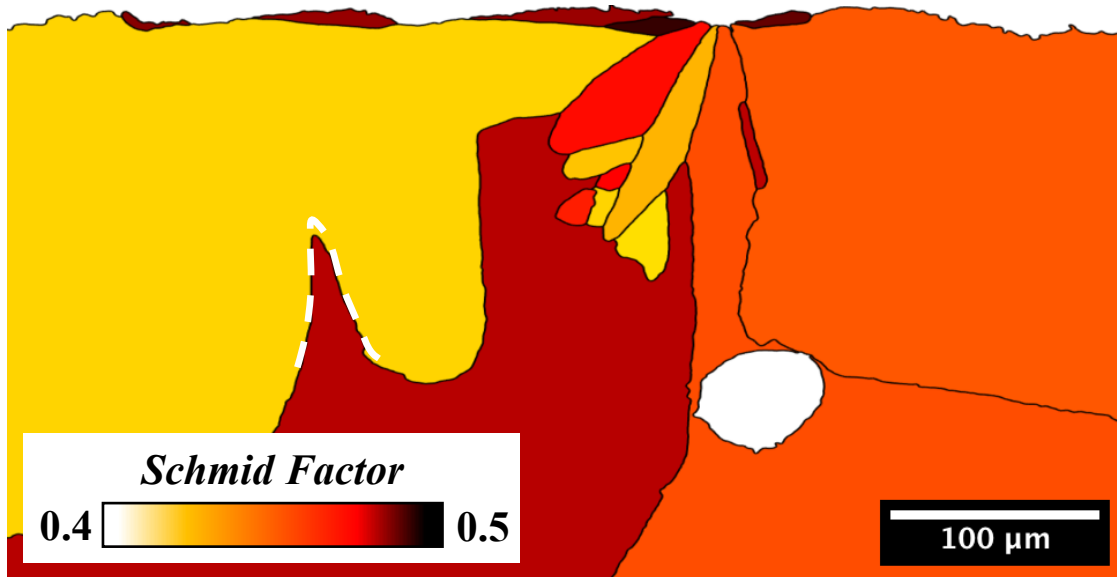
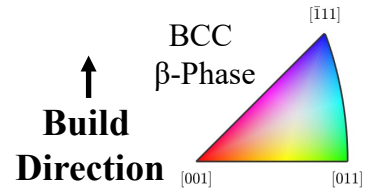
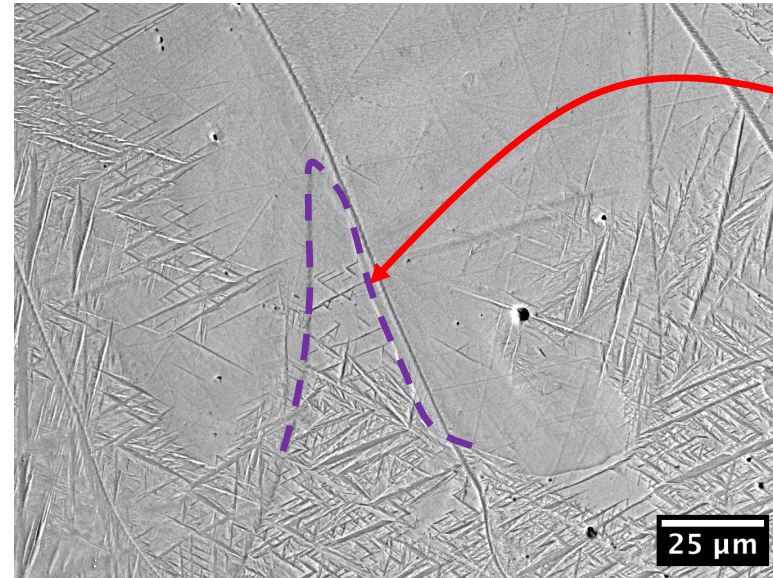
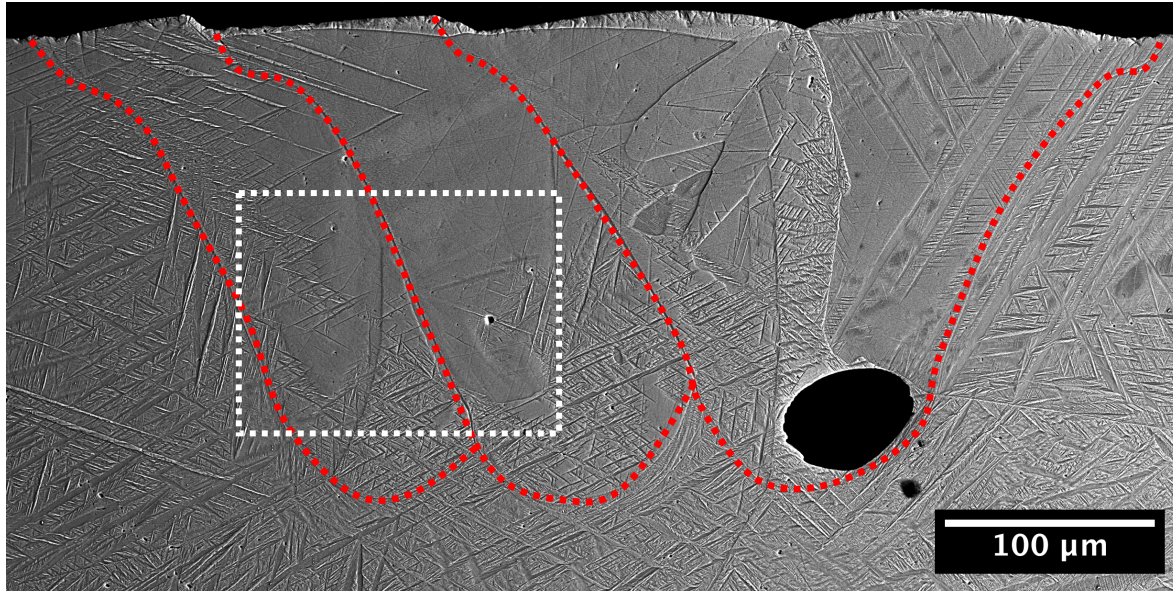
139W Triple Hit



Cooled to RT before next spot-melt

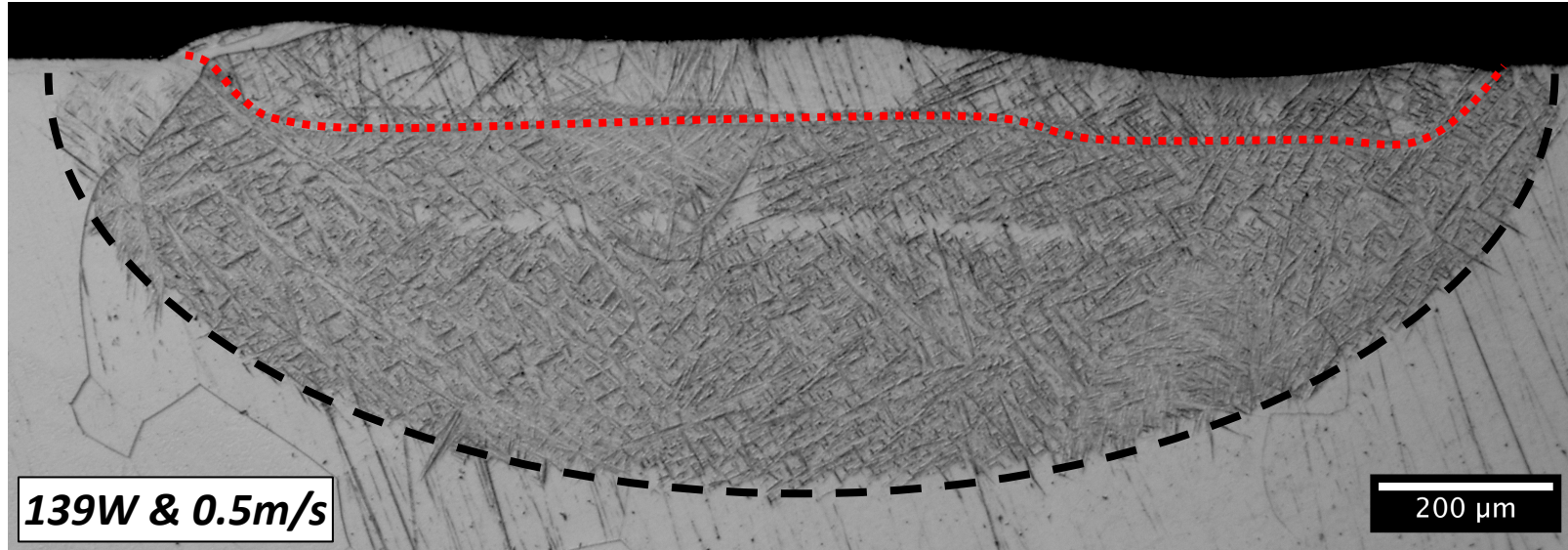


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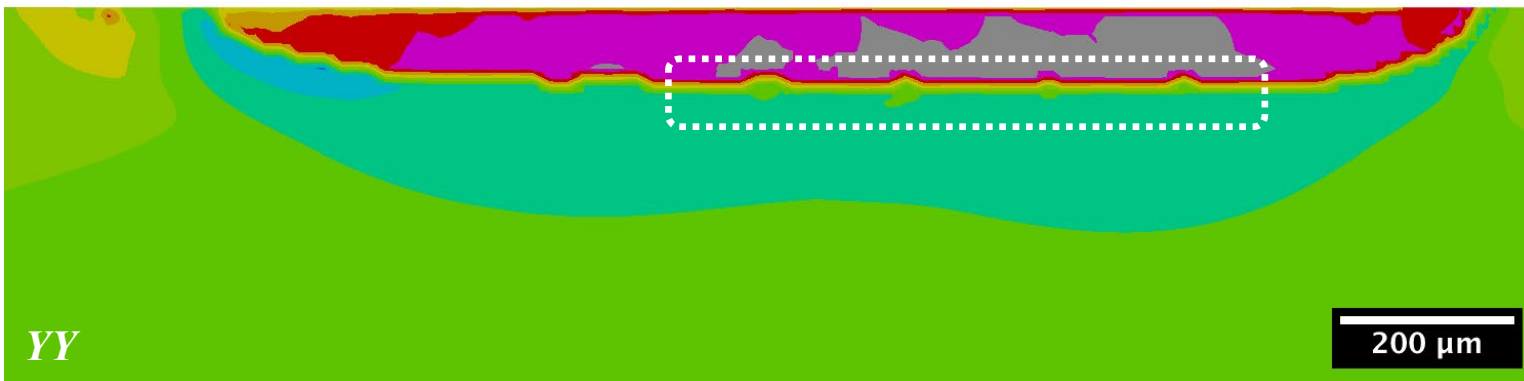
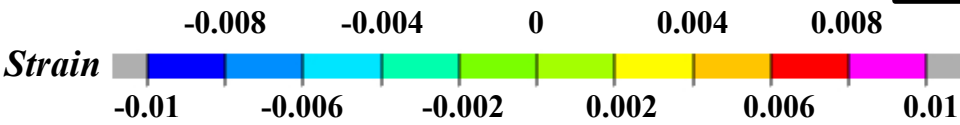
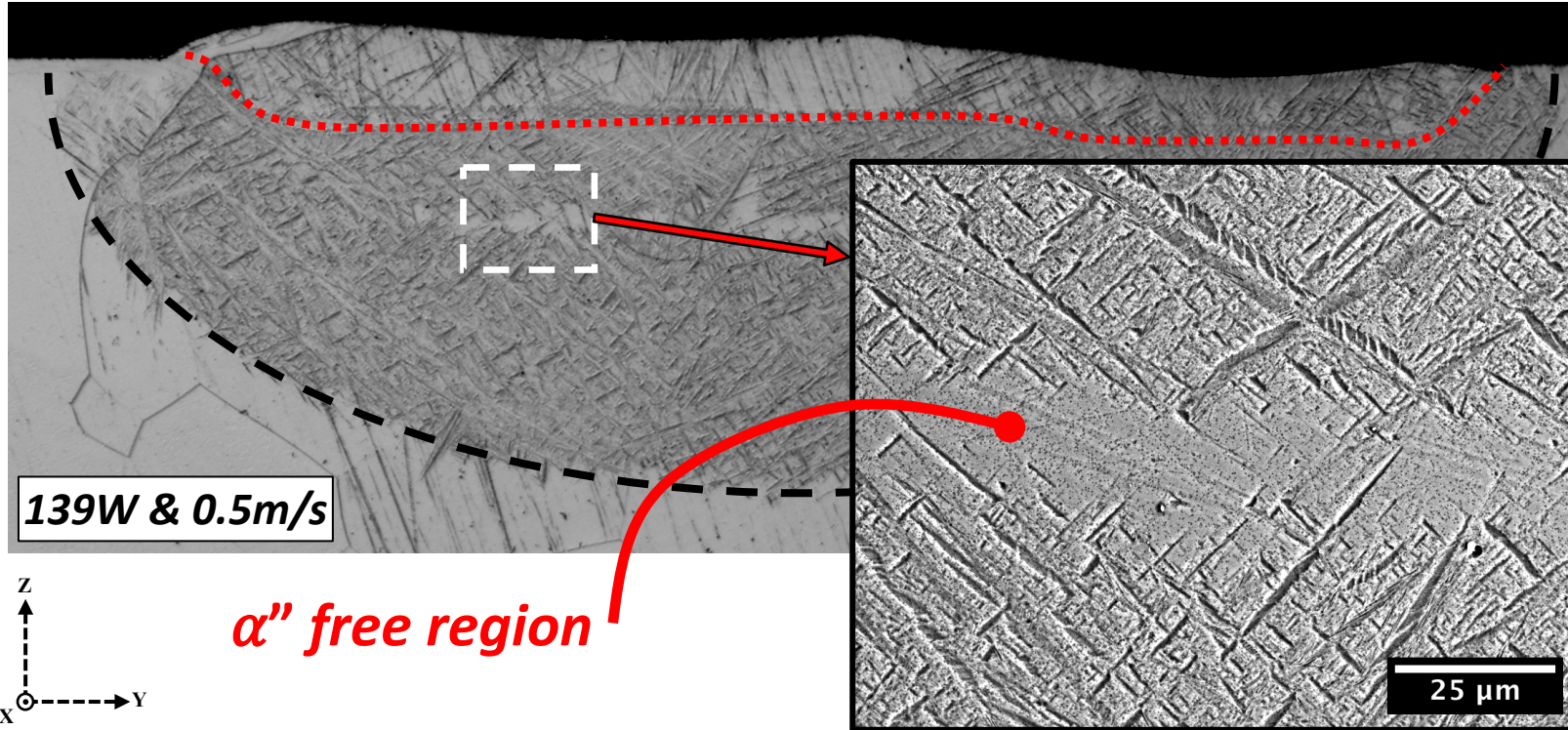
Rasters

Travel Direction →



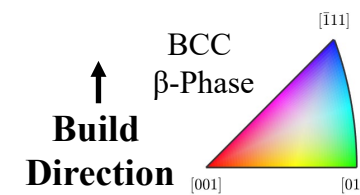
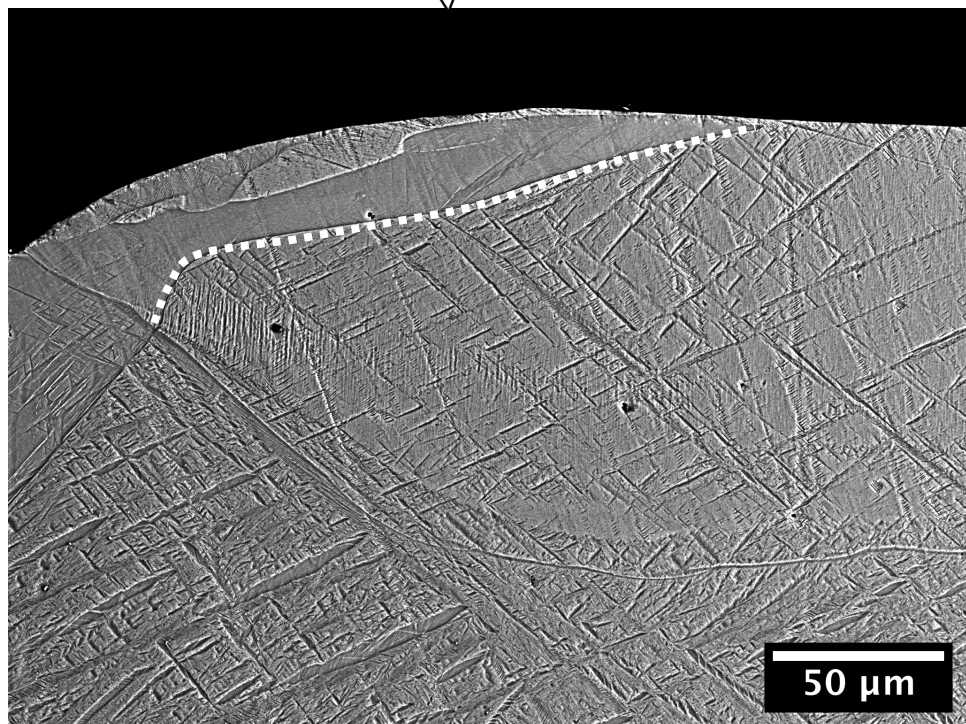
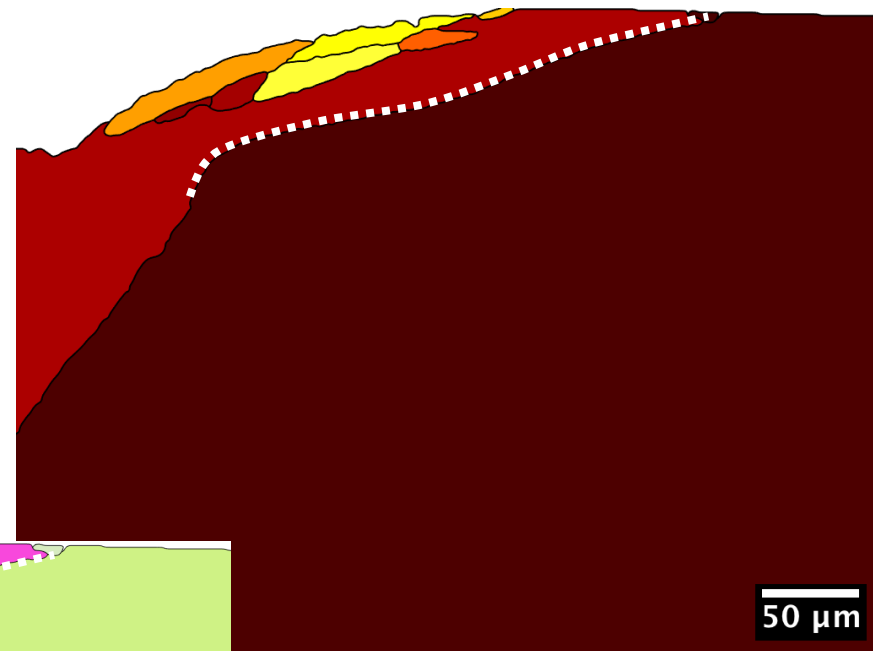
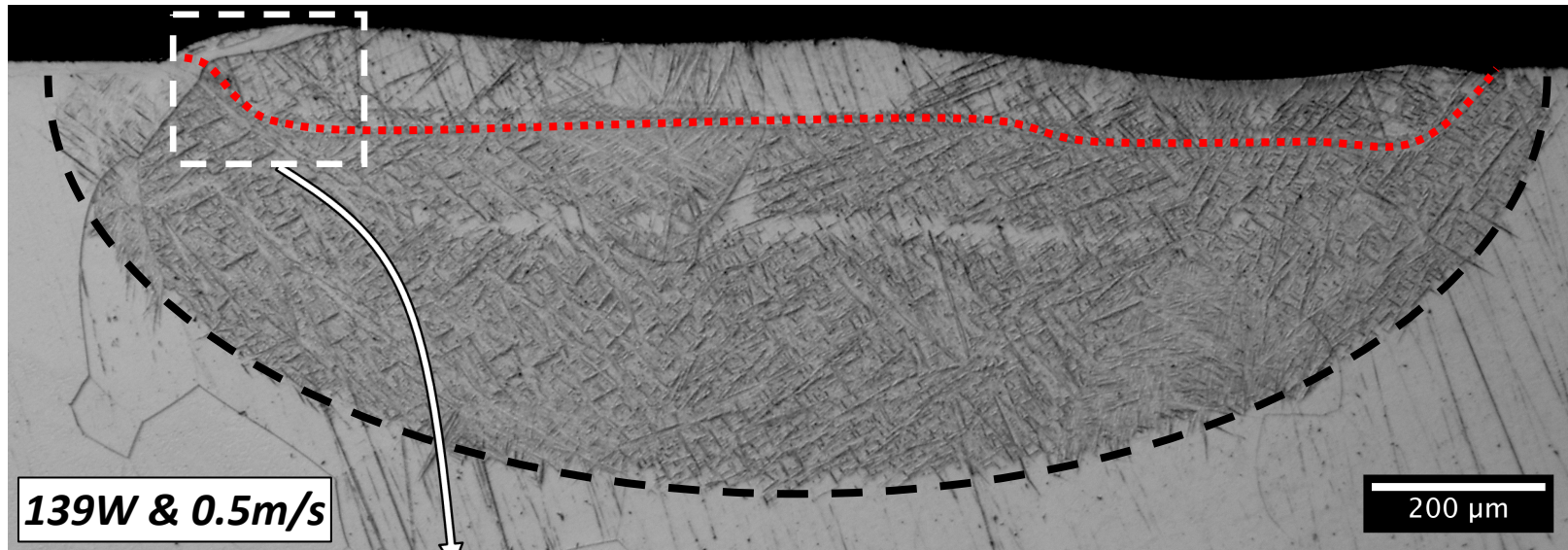
Rasters

Travel Direction →



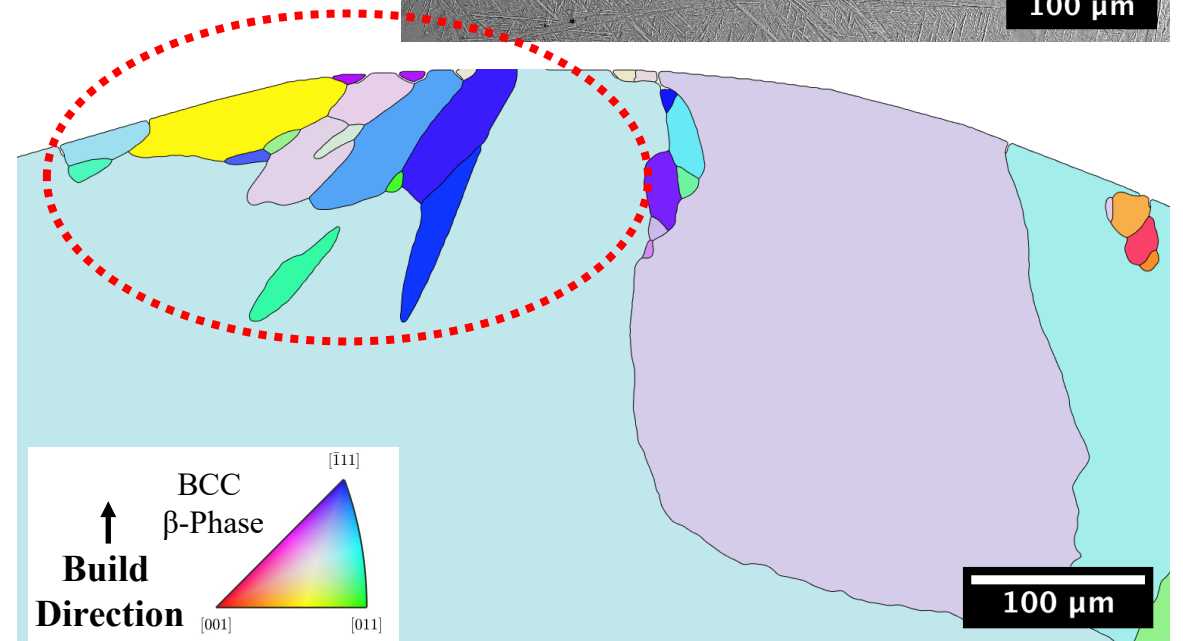
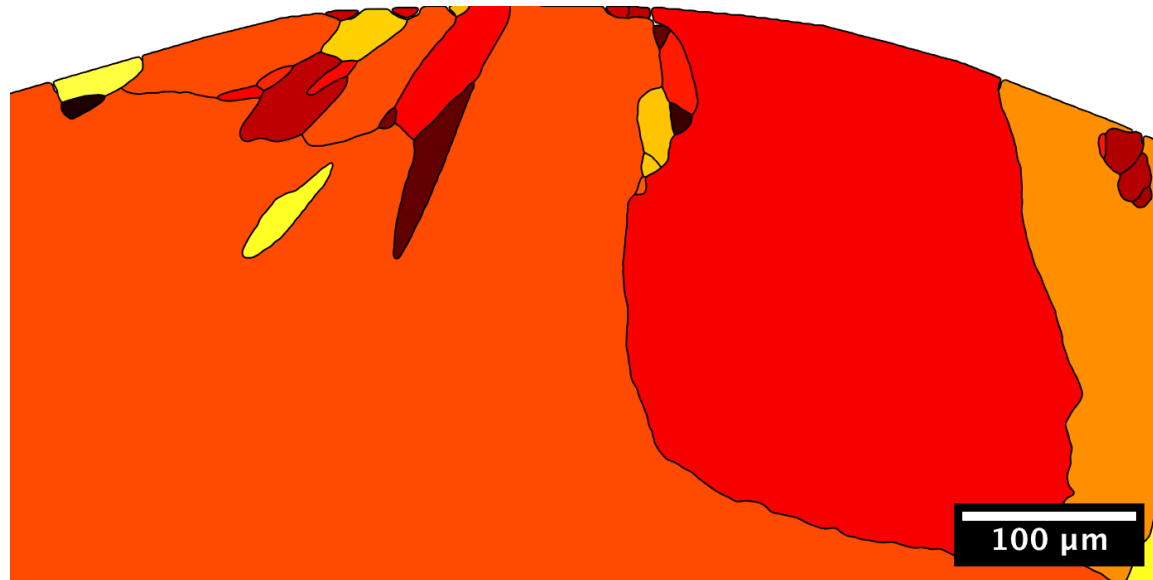
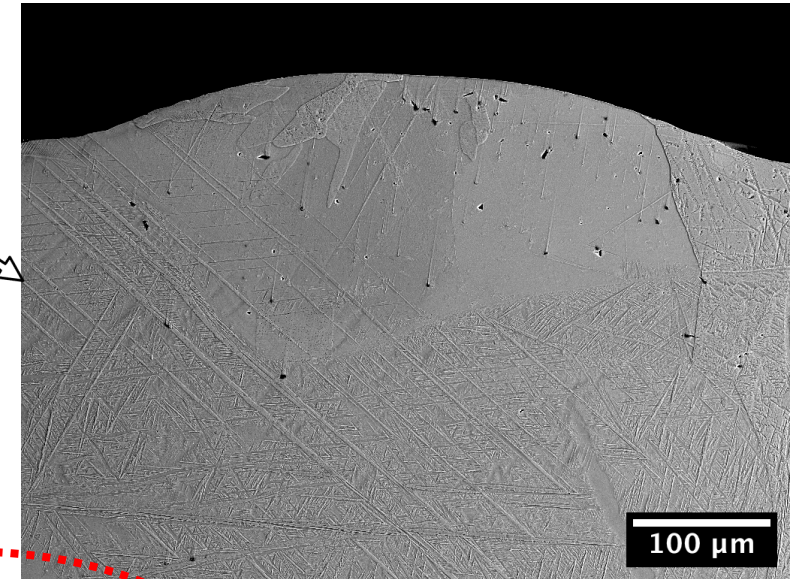
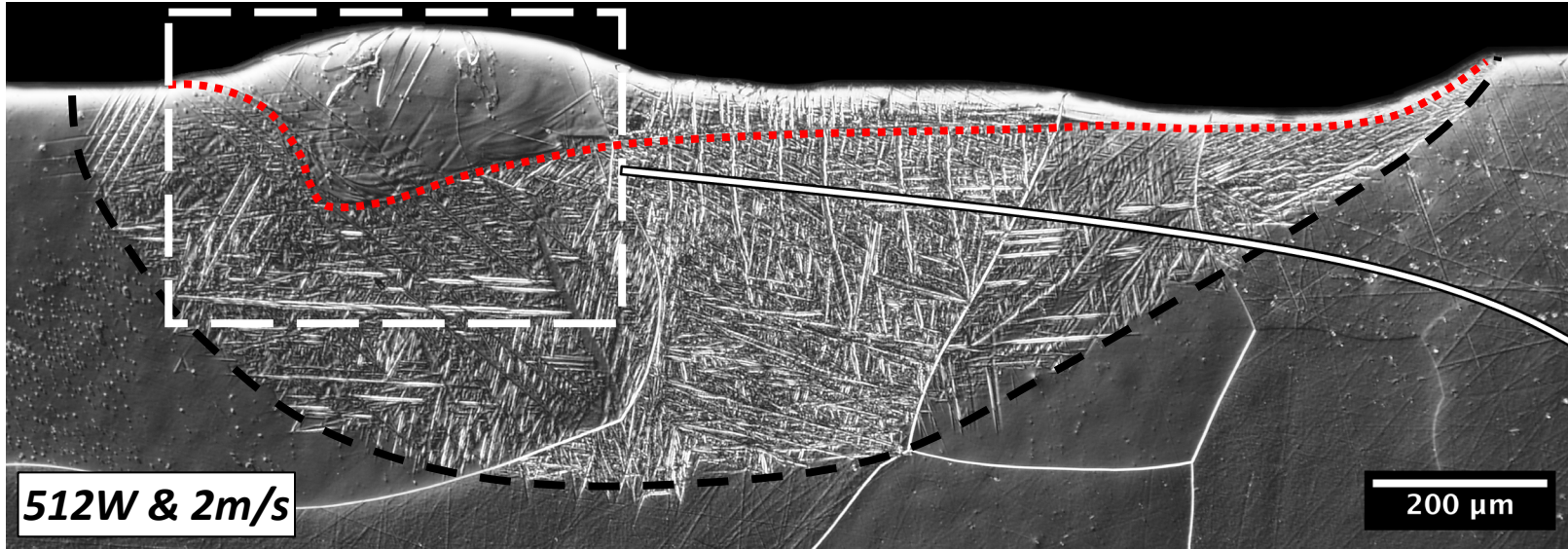
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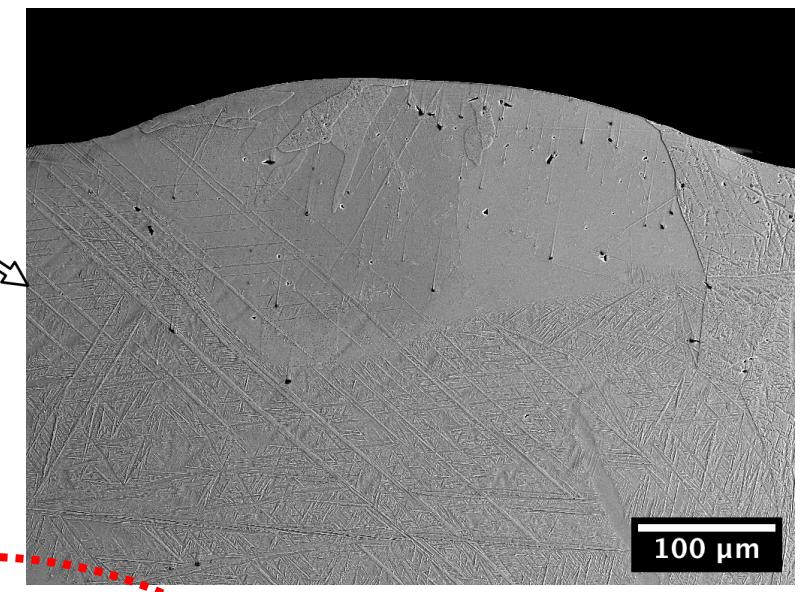
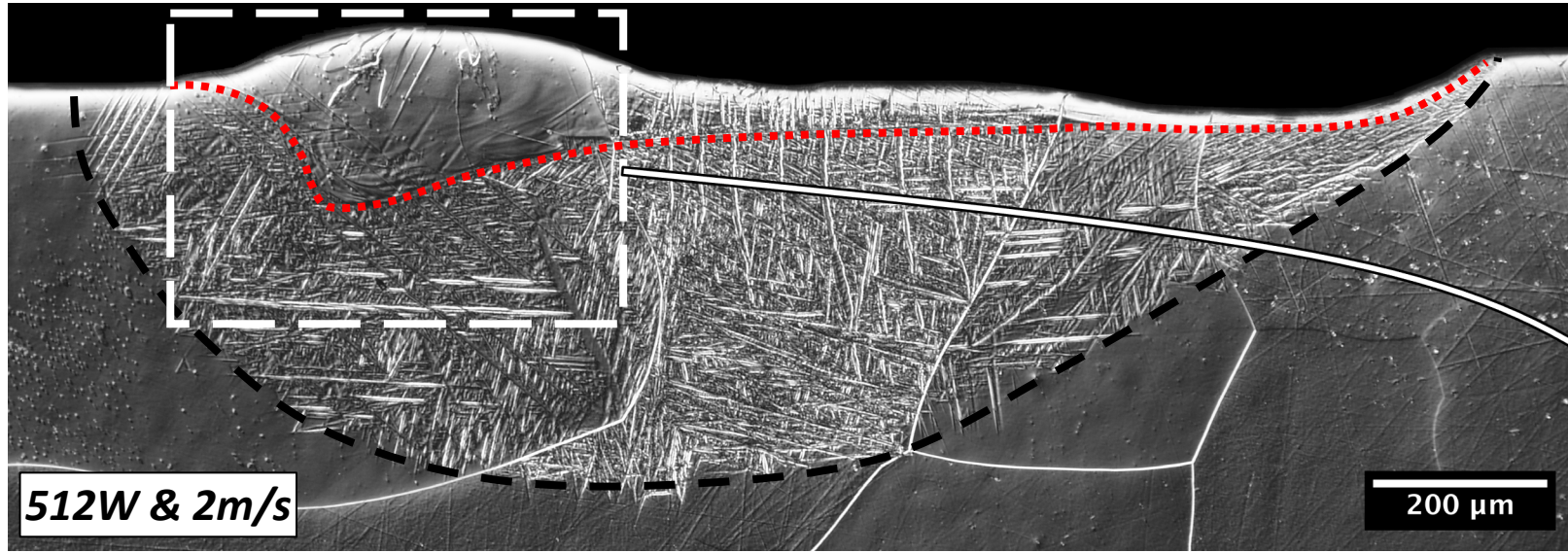
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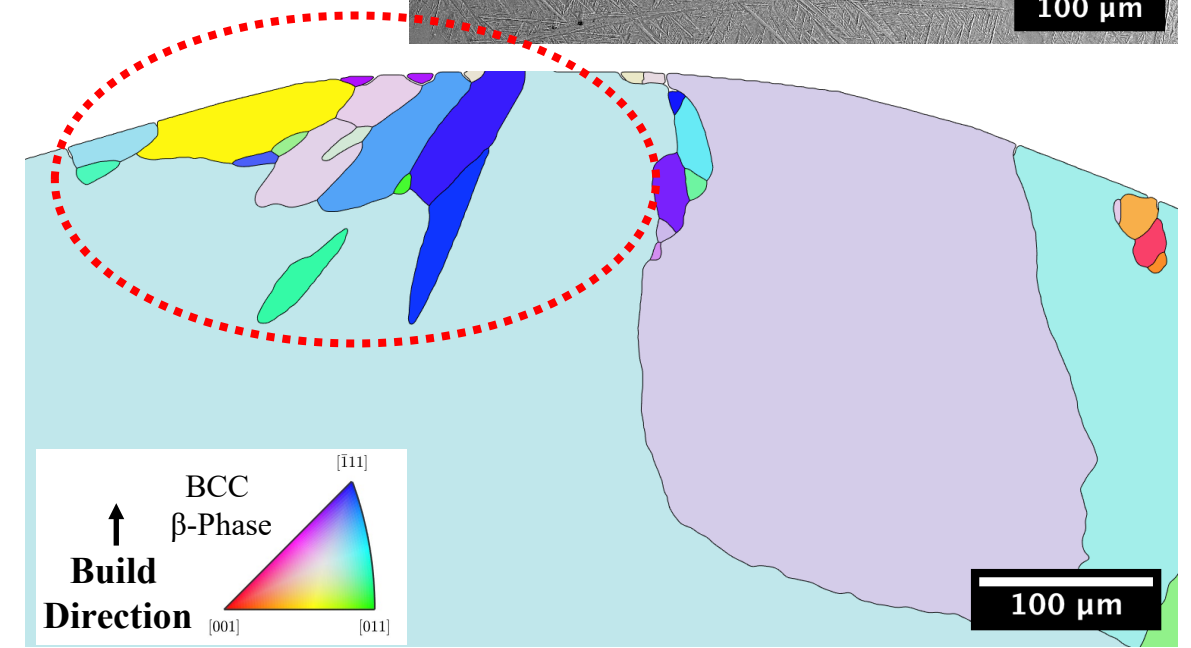
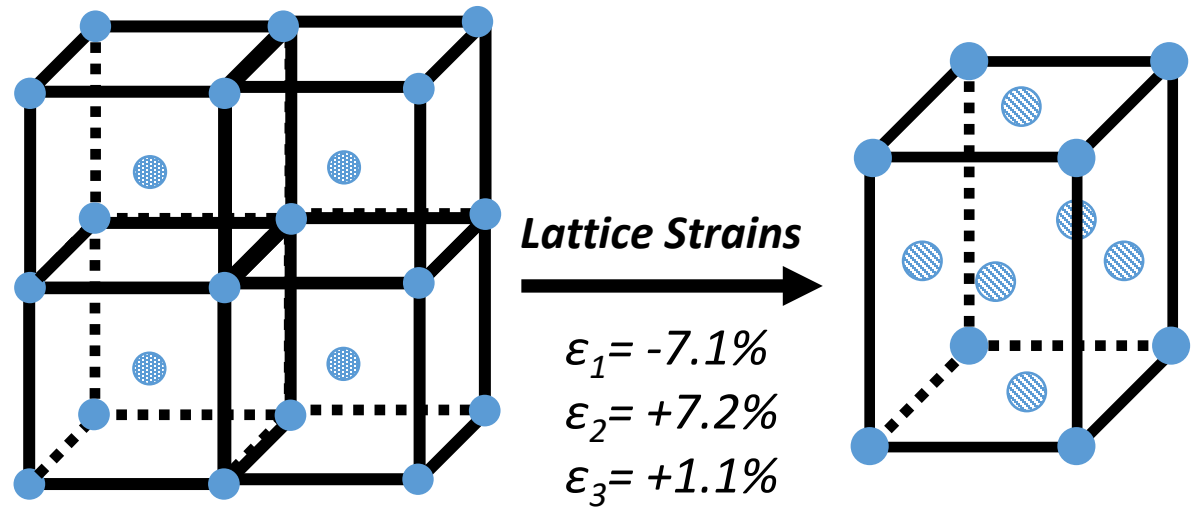


Rasters

Travel Direction →

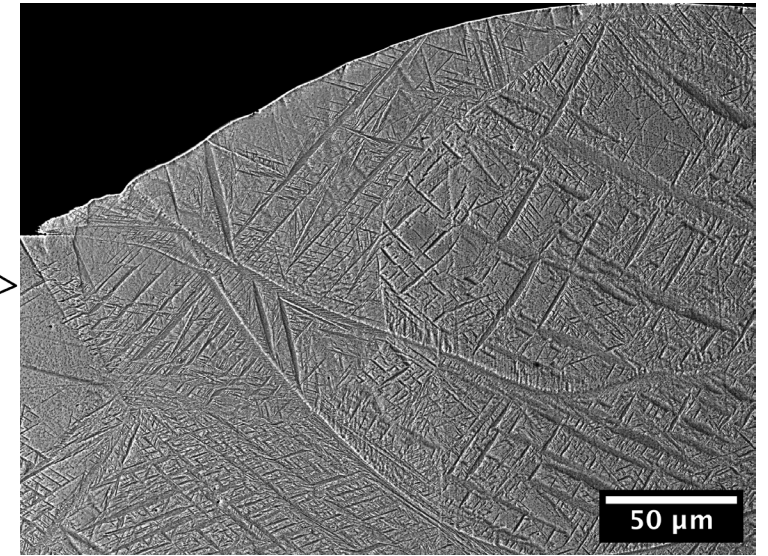
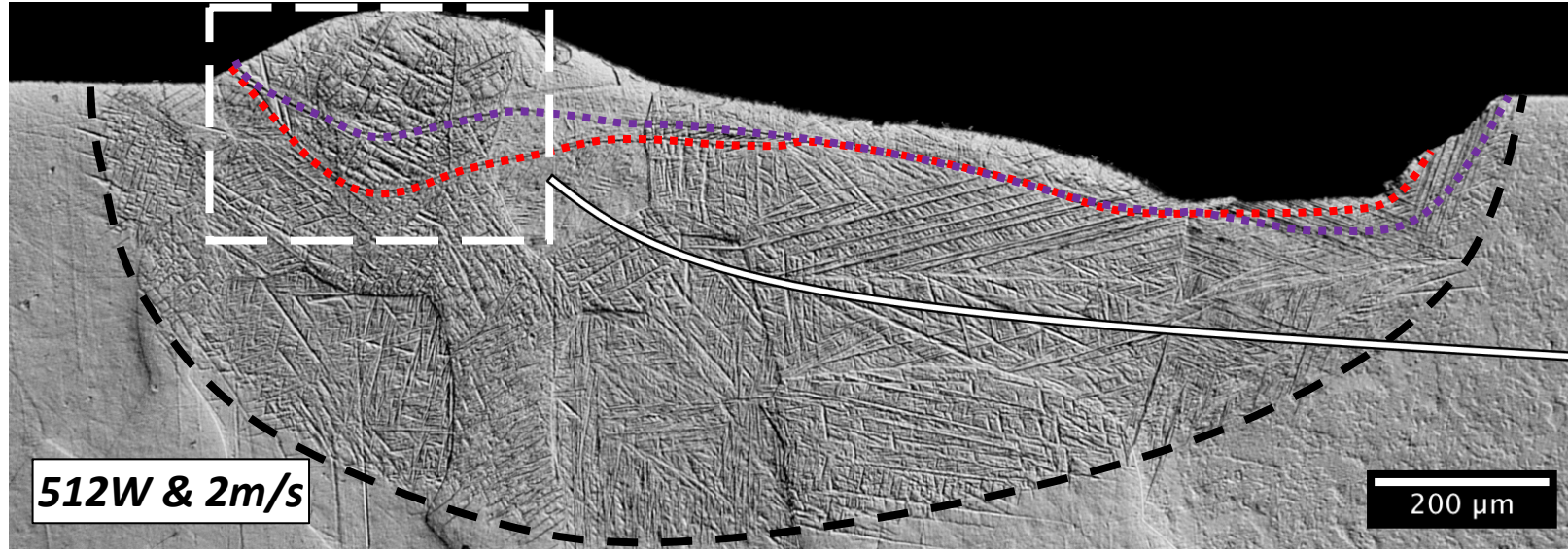
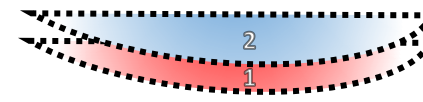


Decreased grain size increases stress necessary for TRIP

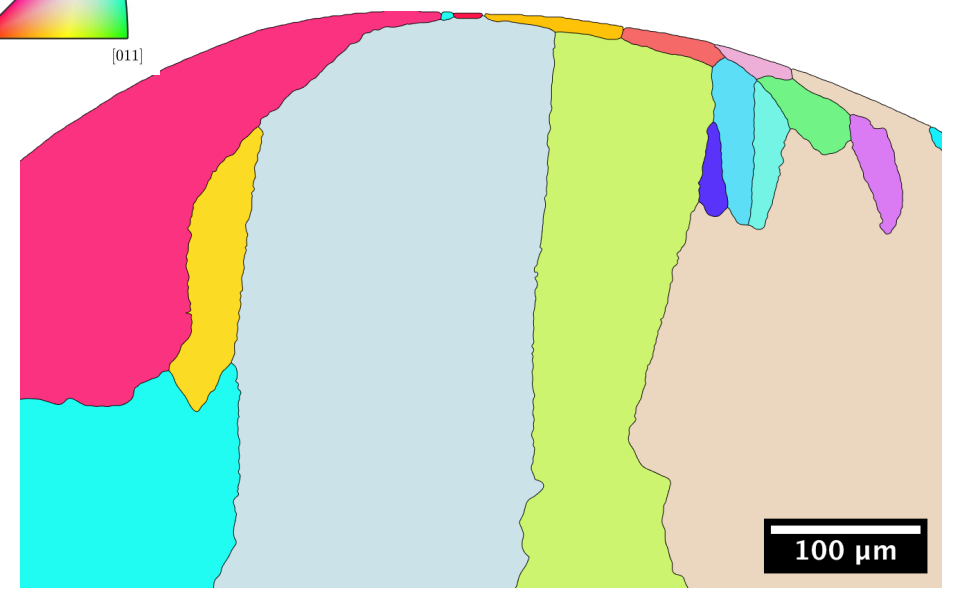
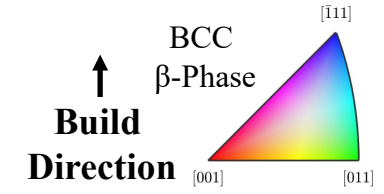


Remelted Rasters

Travel Direction →



Removal of small grains reduces triggering strain for TRIP



Funding & Acknowledgements

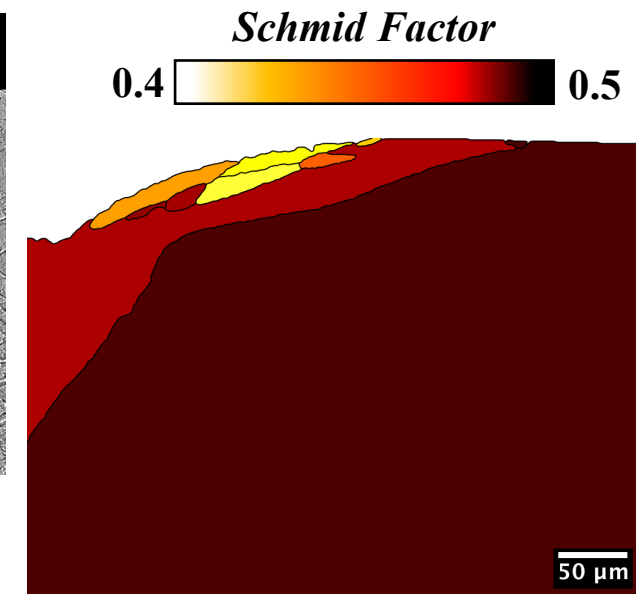
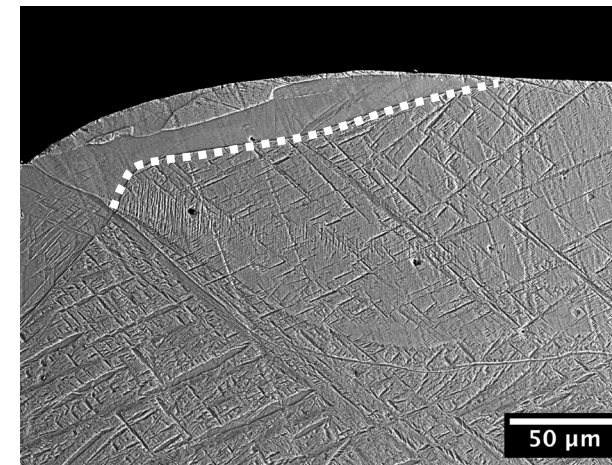
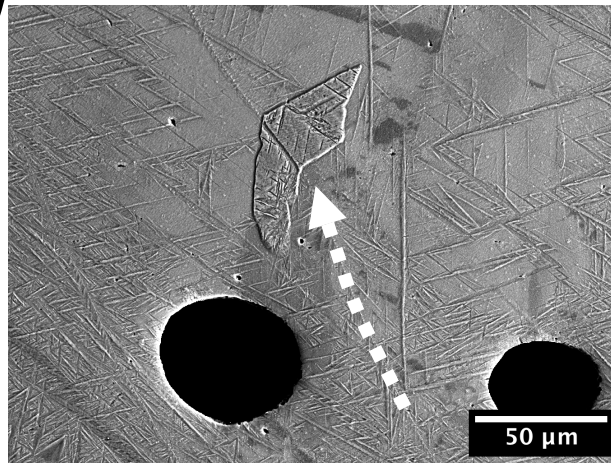
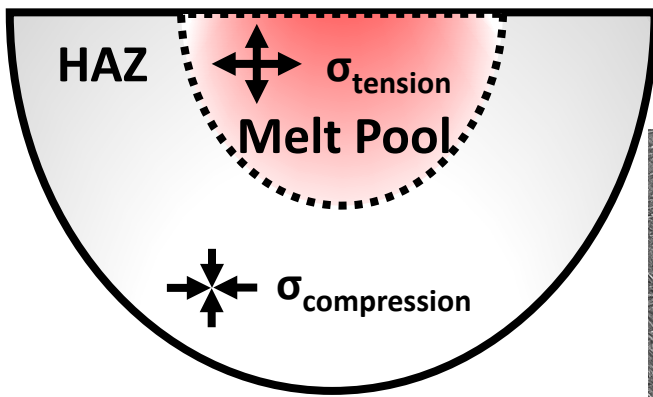


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TRIP is influenced by processing and microstructural features

Melt-pool size
Thermal cycling

Schmid Factor
Grain Size



Accommodation of residual stresses/strains in Ti-1023 may produce crack-free parts with tuned microstructures and properties.